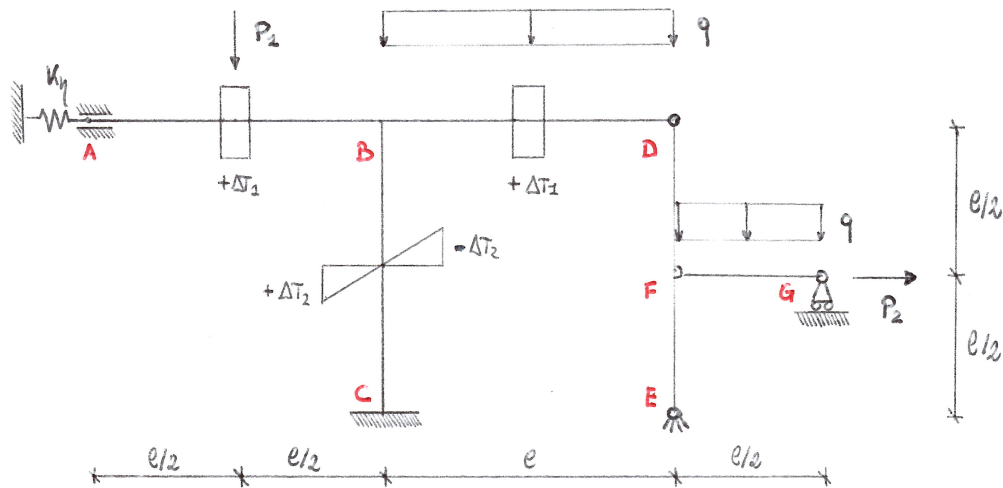




Dati:

$$P_1 = 21 qe$$

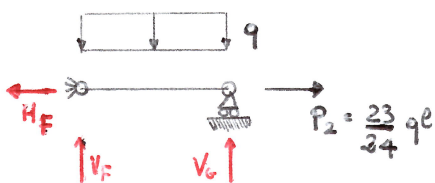
$$P_2 = \frac{23}{24} qe$$

$$\alpha \Delta T_1 = \frac{1}{6} \frac{qe^3}{EI}$$

$$\frac{\alpha \Delta T_2}{h} = \frac{1}{8} \frac{qe^2}{EI}$$

$$K_A = \frac{1}{12} \frac{EI}{e^3}$$

- Si osserva come l'asta FG sia un'appendice isostatica e può quindi essere risolta con gli equilibri e "staccata" dalla struttura principale:

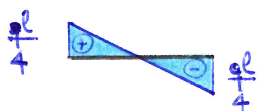


$$V_F = V_G = \frac{qe}{4}$$

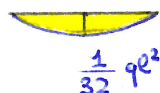
$$H_F = \frac{23}{24} qe$$

grafici delle azioni interne:

Taglio.



Momento.



Azione Assiale



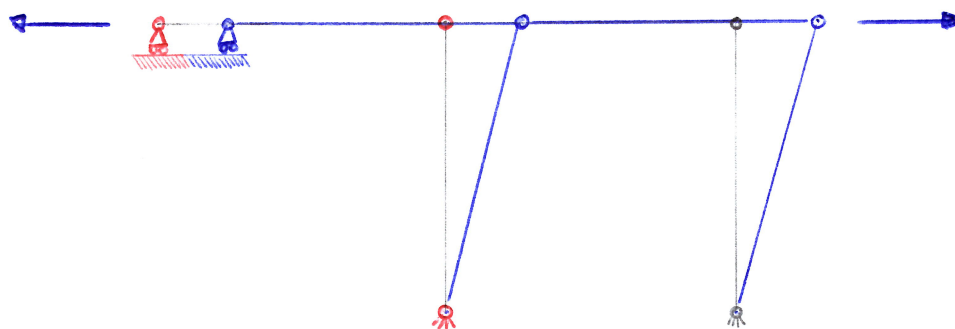
- Si valuta quindi il grado di iperstaticità della struttura:

$$G.d.V = 2 + 1 + 3 + 2 + 2 = 10$$

$$G.d.L = 2 \times 3 = 6$$

⇒ STRUTTURA 4 VOLTE IPERSTATICA

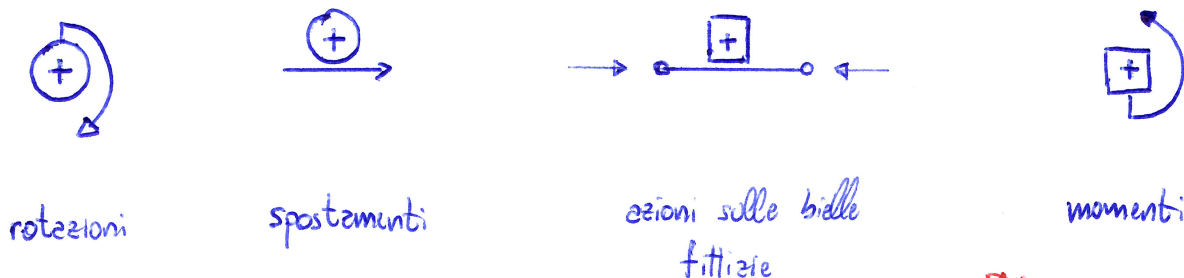
- Si valuta se il telaio sia a nodi fissi o spostabili:



OSSERVAZIONE: IN ROSSO SI SONO RIPORTATI I "VINCOLI MODIFICATI" PER ENFATIZZARE LA DEFORMABILITÀ FLESSIONALE DELLE ASTE CHE COMPLEGONO LA STRUTTURA.

- ⇒ Si individua chiaramente un possibile cinetismo per le aste AB e BD.
Il telaio è quindi a nodi spostabili.

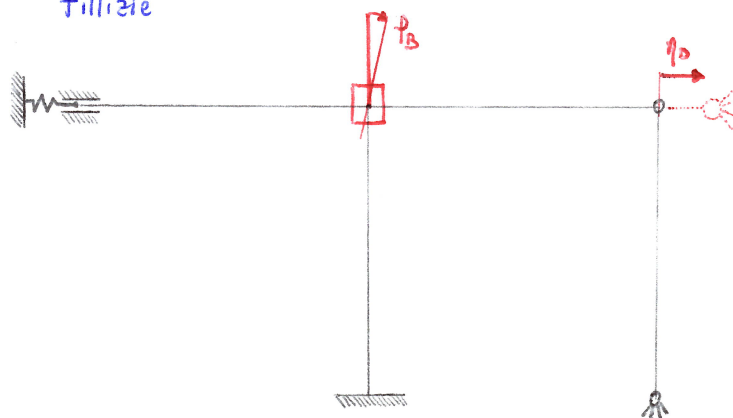
- Convenzioni adottate per la risoluzione del telaio:



- Si decide di risolvere il telaio adottando il metodo degli spostamenti, le incognite sono:

* ϕ_B

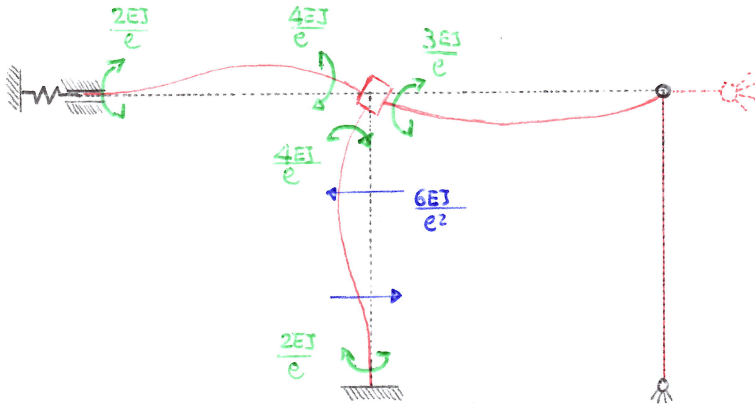
* η_D



Da cui il sistema risolvete (SISTEMA DELLE EQUAZIONI DI EQUILIBRIO)

$$\begin{cases} \sum M_B = 0 \\ \sum R_D = 0 \end{cases} \quad \begin{cases} M_{BB} \varphi_B + M_{BD} \eta_D + M_o = 0 \\ h_{DB} \varphi_B + h_{DD} \eta_D + h_{D0} = 0 \end{cases}$$

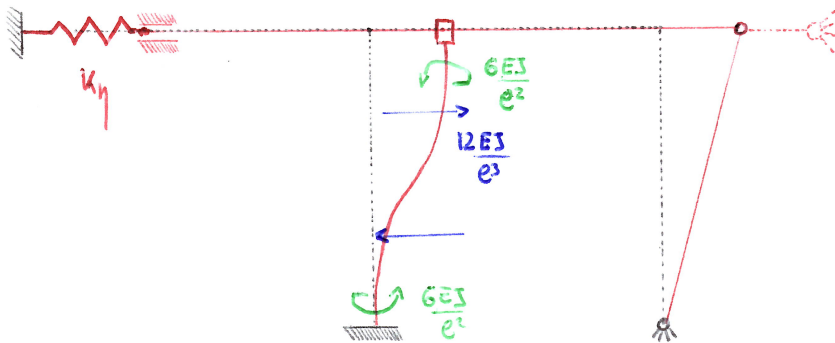
• CASO 1: $\varphi_B = 1$



$$M_{BB} = + 11 \frac{EJ}{e}$$

$$h_{DB} = + 6 \frac{EJ}{e^2}$$

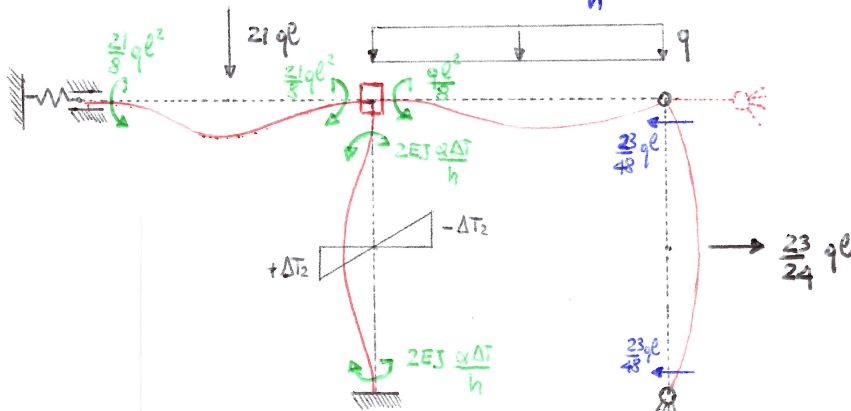
• CASO 2: $\eta_D = 1$



$$M_{DD} = - 6 \frac{EJ}{e^2}$$

$$\begin{aligned} h_{DD} &= - 12 \frac{EJ}{e^3} - k_{\eta} \cdot 1 \\ &= - 12 \frac{EJ}{e^3} - \frac{1}{12} \frac{EJ}{e^3} \\ &= - \frac{145}{12} \frac{EJ}{e^3} \end{aligned}$$

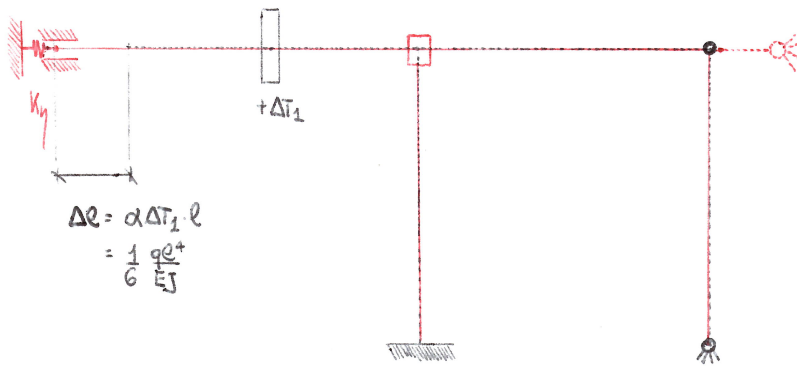
• CASO 3: $P_1 \neq 0; P_2 \neq 0; q \neq 0; \frac{\alpha \Delta T_2}{h} \neq 0$



$$\begin{aligned} M_{DD}^3 &= + \frac{21}{8} qe^2 - 2EJ \cdot \frac{1}{8} \frac{qe^2}{EJ} - \frac{qe^2}{8} \\ &= + \frac{9}{4} qe^2 \end{aligned}$$

$$h_{DD}^3 = + \frac{23}{48} qe$$

• CASO 4: $\Delta T_1 \neq 0$



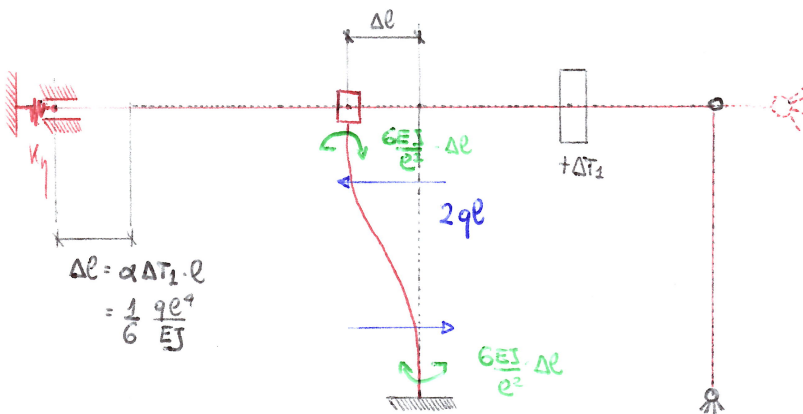
$$M_{BO}^4 = 0$$

$$h_{DO}^4 = + K_h \cdot \Delta l$$

$$= + \frac{1}{6} \frac{q l^4}{EJ} \cdot \frac{1}{l} \frac{EJ}{l^3}$$

$$= + \frac{1}{72} q l$$

• CASO 5: $\Delta T_1 \neq 0$



$$M_{BO}^5 = \frac{6EJ}{l^2} \cdot \frac{1}{6} \frac{q l^4}{EJ}$$

$$= q l^2$$

$$h_{DO}^5 = + 2 q l + K_h \cdot \Delta l$$

$$= + 2 q l + \frac{1}{72} q l$$

$$= \frac{145}{72} q l$$

Sistema risolvete:

$$\begin{cases} 11 \frac{EJ}{l} \varphi_B - \frac{6EJ}{l^2} \eta_D + \frac{9}{4} q l^2 + 0 + q l^2 = 0 & 1) \\ 6 \frac{EJ}{l^2} \varphi_B - \frac{145EJ}{12 l^3} \eta_D + \frac{23}{48} q l + \frac{1}{72} q l + \frac{145}{72} q l = 0 & 2) \end{cases}$$

moltiplico l'equazione 2) per $\frac{11}{6} l$ e la sottraggo alla 1)

$$- \frac{6EJ}{l^2} \eta_D + \frac{145}{12} - \frac{11}{6} \frac{EJ}{l^2} \eta_D + \frac{13}{4} q l^2 - \frac{361}{144} \cdot \frac{11}{6} q l^2 = 0$$

$$\frac{1163}{72} \frac{EJ}{l^2} \eta_D - \frac{1163}{864} q l^2 = 0 \rightarrow \eta_D = \frac{1}{12} \frac{q l^4}{EJ}$$

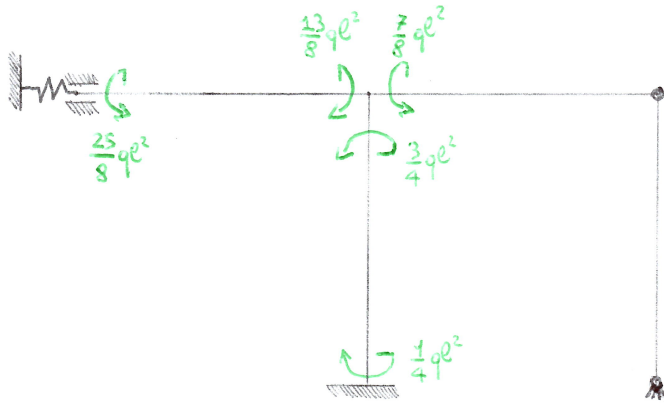
sostituendo η_D in 1) ricevo:

$$\varphi_B = - \frac{1}{4} \frac{q l^3}{EJ}$$

Da cui in conclusione:

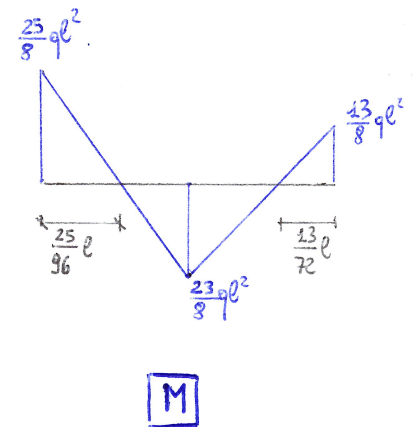
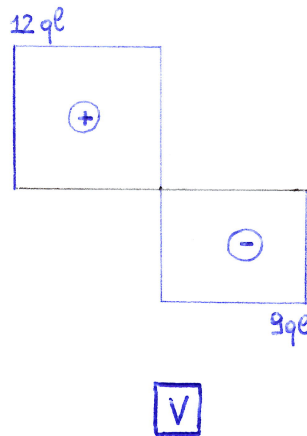
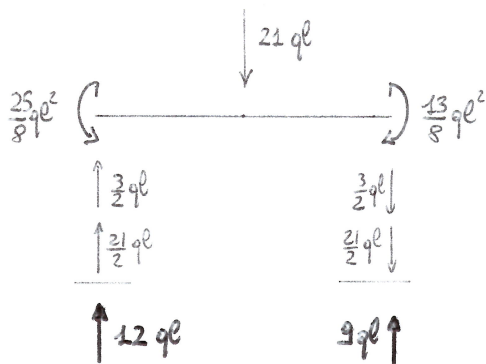
$$\begin{cases} \theta_B = -\frac{1}{4} \frac{ql^3}{EI} \\ \eta_D = +\frac{1}{12} \frac{ql^4}{EI} \end{cases}$$

- Si passa quindi al calcolo delle azioni interne

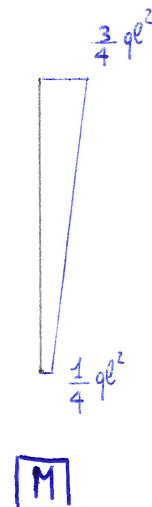
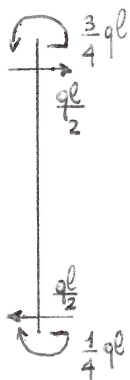


SOMMANDO I CONTRIBUTI
DAI 5 CASI PRECEDENTI
SI OTTENGONO I SEGUENTI
MOMENTI ALLE ESTREMITÀ
DELLE ASTE

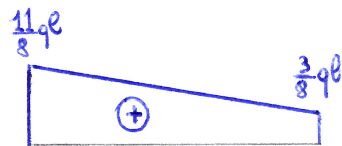
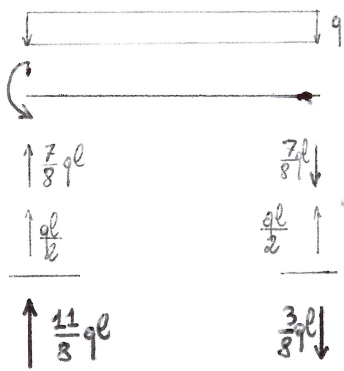
ASTA AB



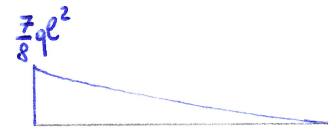
ASTA BC



ASTA BD

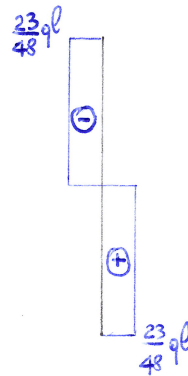
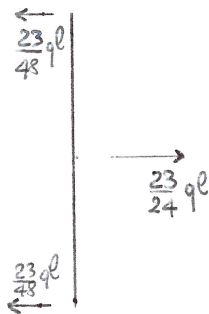


V

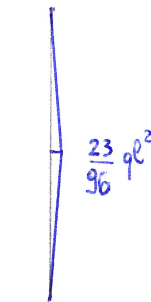


M

ASTA DE



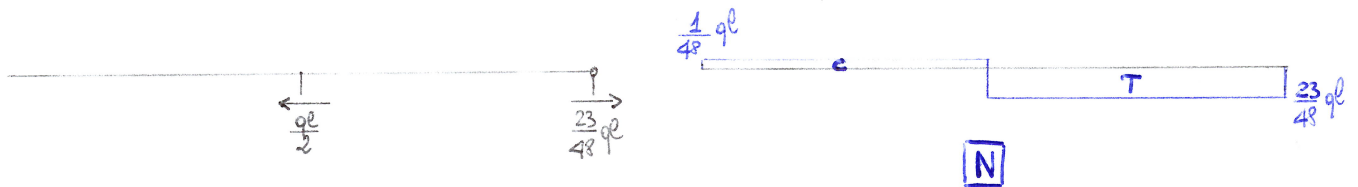
V



M

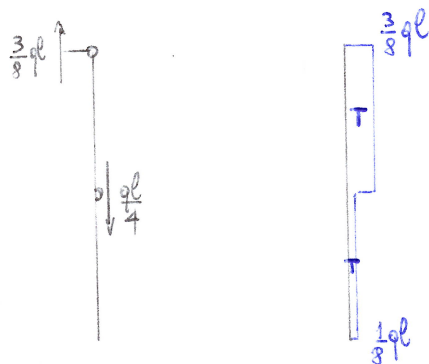
AZIONI ASSIALI:

ASTE AB + BD



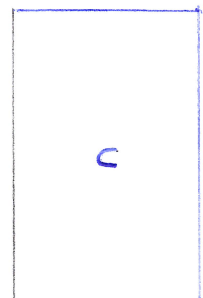
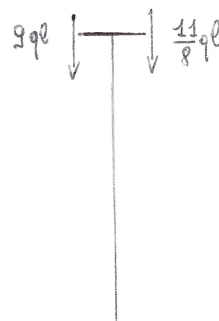
N

ASTA DE



N

ASTA BC

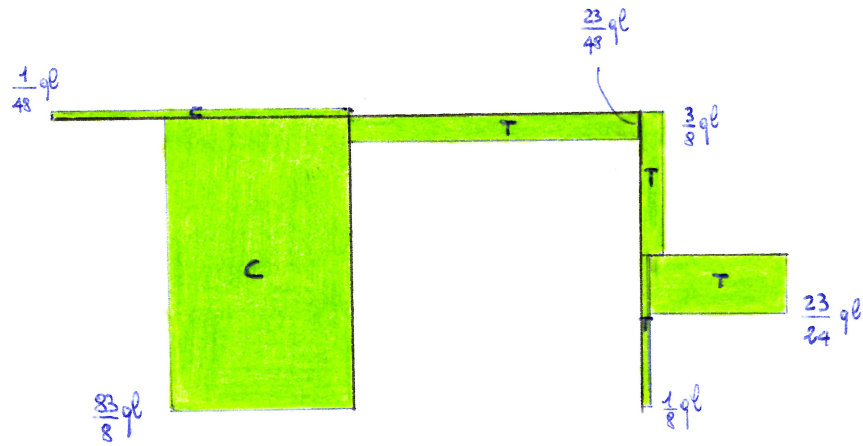


N

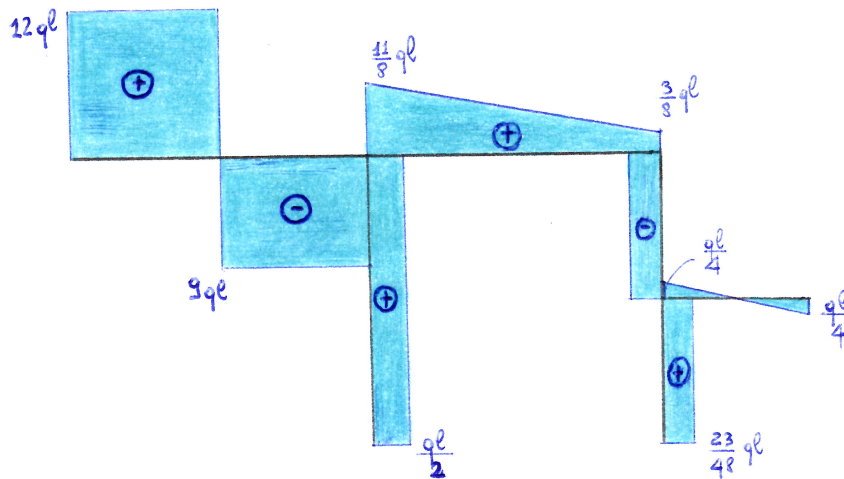
$\frac{83}{8} ql$

• Grafici finali:

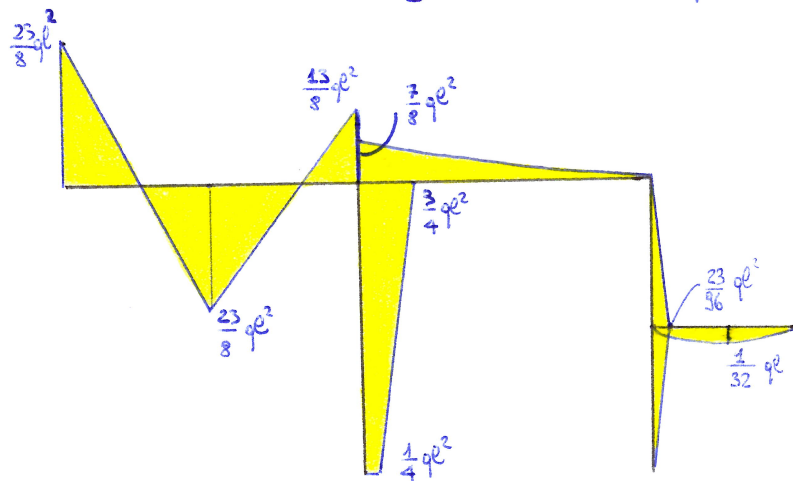
AZIONE
ASSIALE



TAGLIO



MOMENTO

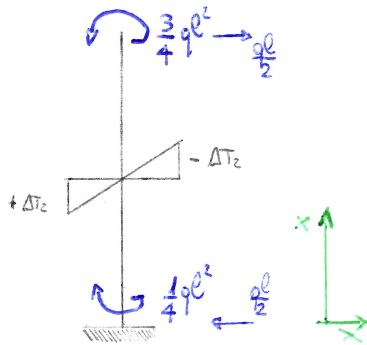


• Deformata qualitativa

Per il tracciamento della deformata qualitativa è necessario valutare:

1. La deformata dell'asta BC a cause delle variazioni termiche a perfello
2. Spostamenti nodali in A e B

1. DEFORMATA PER ASTA BC



Si valuta il segno della curvatura della trave sfruttando l'equazione della linea elastica:

$$y'' = - \frac{M(x)}{EJ} \pm 2 \frac{\alpha \Delta T}{h}$$

$$M(x) = \frac{1}{4} ql^2 + \frac{ql}{2} x$$

$$y'' = - \frac{1}{EJ} \left[\frac{1}{4} ql^2 + \frac{ql}{2} x \right] + 2 \cdot \frac{1}{8} \frac{ql^2}{EJ}$$

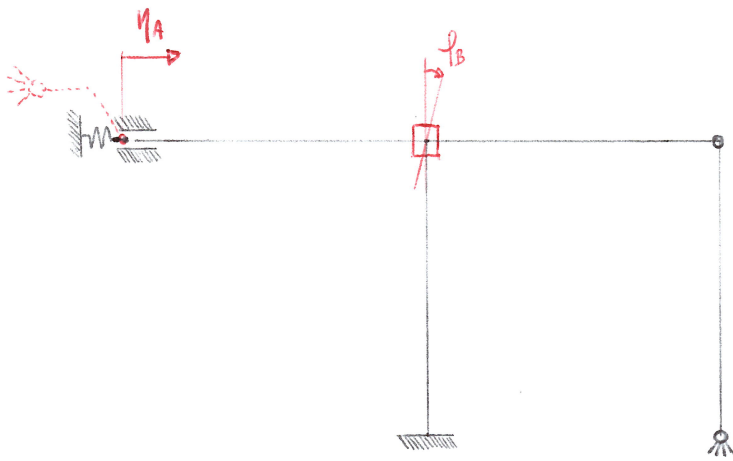
$$y'' EJ = - \frac{1}{4} ql^2 - \frac{ql}{2} x + \frac{1}{4} ql^2$$

$$y'' EJ = - \frac{ql}{2} x \Rightarrow \underline{\underline{\forall x > 0 \quad y'' < 0}}$$

2. SPOSTAMENTI NODALI IN A E B

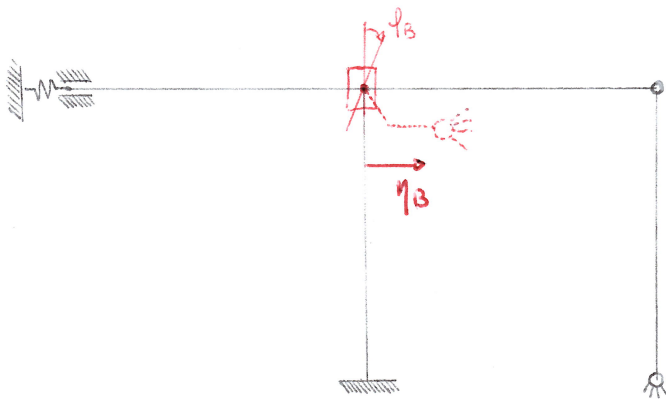
A cause delle variazioni termiche costanti: $\eta_0 \neq \eta_B \neq \eta_A$.

Per valutare gli spostamenti η_A e η_B si può riapplicare il metodo degli spostamenti andando a mettere una volta la bielletta fittizia in A e poi (ripetendo i calcoli) mettendo la bielletta in B.



Incognite:

$$\begin{cases} \eta_A \\ \eta_B \end{cases}$$



Incognite

$$\begin{cases} \eta_B \\ \eta_B \end{cases}$$

Sviluppando i calcoli si ottiene:

$$\begin{cases} \eta_A = -\frac{1}{4} \frac{ql^4}{EJ} \\ \eta_B = -\frac{1}{12} \frac{ql^4}{EJ} \end{cases}$$

Tuttavia gli spostamenti in A e B si possono valutare anche in modo più veloce. Infatti nell'ipotesi che $EA \rightarrow \infty$ si può scrivere:

$$\eta_A = \eta_D - \alpha \Delta T_1 \cdot l_{AB} - \alpha \Delta T_2 \cdot l_{BD} = \frac{1}{12} \frac{ql^4}{EJ} - \frac{1}{6} \frac{ql^3}{EJ} l - \frac{1}{6} \frac{ql^3}{EJ} l = -\frac{1}{4} \frac{ql^4}{EJ}$$

$$\eta_B = \eta_D - \alpha \Delta T_2 l_{BD} = \frac{1}{12} \frac{ql^4}{EJ} - \frac{1}{6} \frac{ql^3}{EJ} l = -\frac{1}{12} \frac{ql^4}{EJ}$$

Deformata qualitativa:

