

TECNICA DELLE COSTRUZIONI

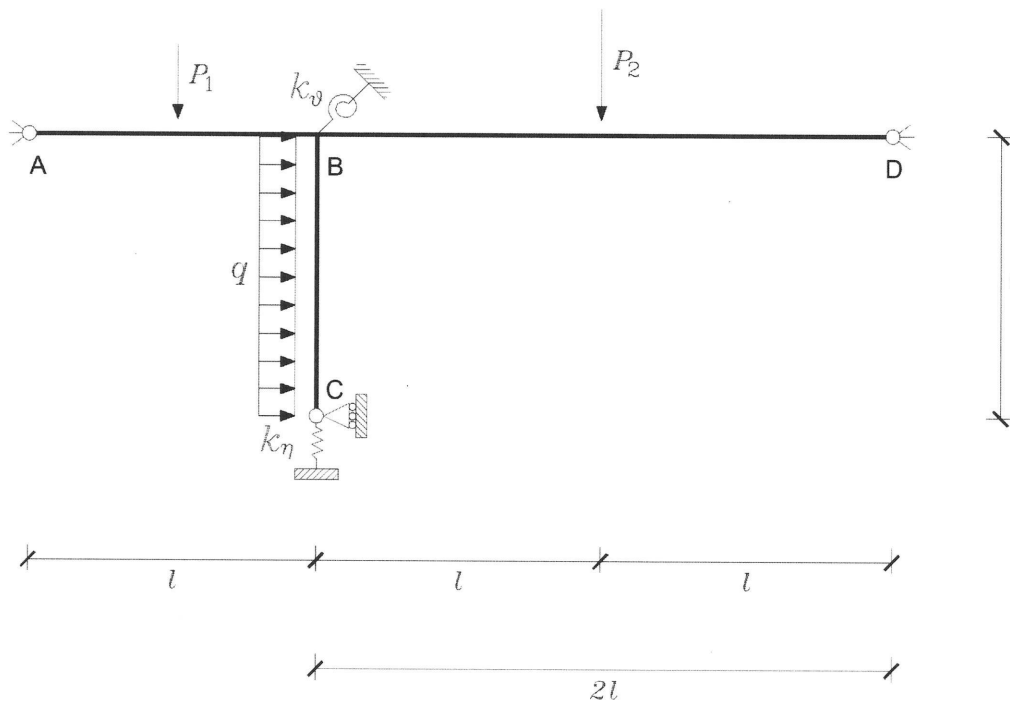
TEMA ESAME DEL 19 GIUGNO 2017

DOCENTE: PROF. FAUSTO MINELLI

ESERCITATORE: ING. LUCA FACCONI

DURATA: 2 ORE

Esercizio



$$K_{\theta} = \frac{13 EJ}{4 l}$$

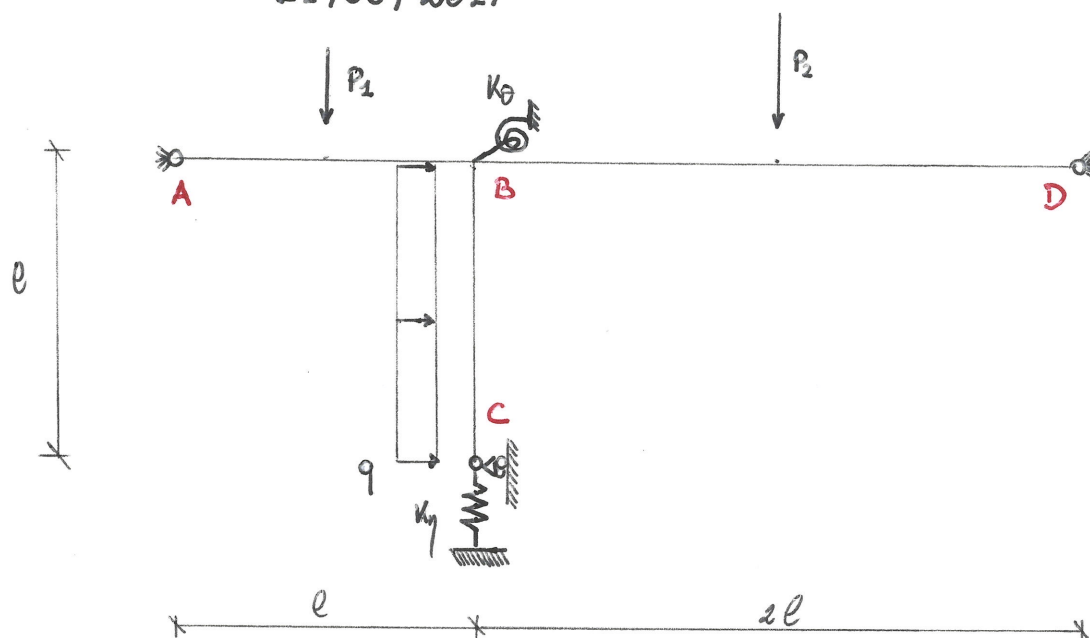
$$K_{\eta} = \frac{45 EJ}{8 l^3}$$

$$P_1 = 4ql$$

$$P_2 = 5ql$$

Dato il telaio in figura, si richiedono i grafici di:

1. Momento flettente (con il valore e la posizione dei massimi);
2. Taglio;
3. Azione assiale;
4. Deformata qualitativa con posizione dei flessi.



Dati:

$$K_{\theta} = \frac{13}{4} \frac{EJ}{e}$$

$$P_1 = 4 qe$$

$$K_y = \frac{45}{8} \frac{EJ}{e^3}$$

$$P_2 = 5 qe$$

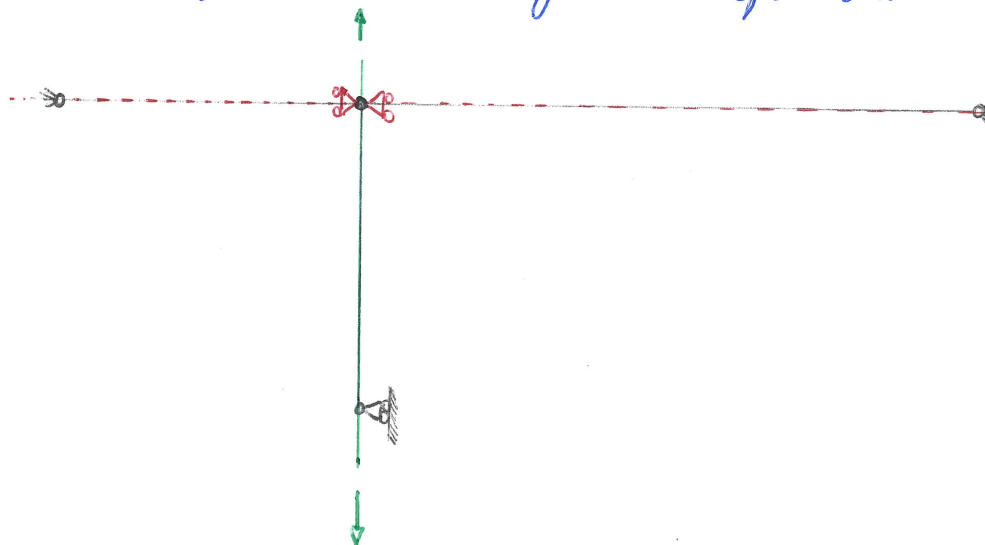
- Si valuta il grado di iperstaticità della struttura:

$$G.d.V. = 2 + 1 + 2 = 5$$

$$G.d.L. = 3 \cdot 1 = 3$$

→ struttura 2 volte iperstatica

- Si valuta se il telero sia a nodi fissi o spostabili:



→ si osserva un possibile circuitismo per l'asta ec. Il telero è a nodi spostabili

• Convenzioni adottate nella risoluzione del telaio:



ROTAZIONI



SPOSTAMENTI



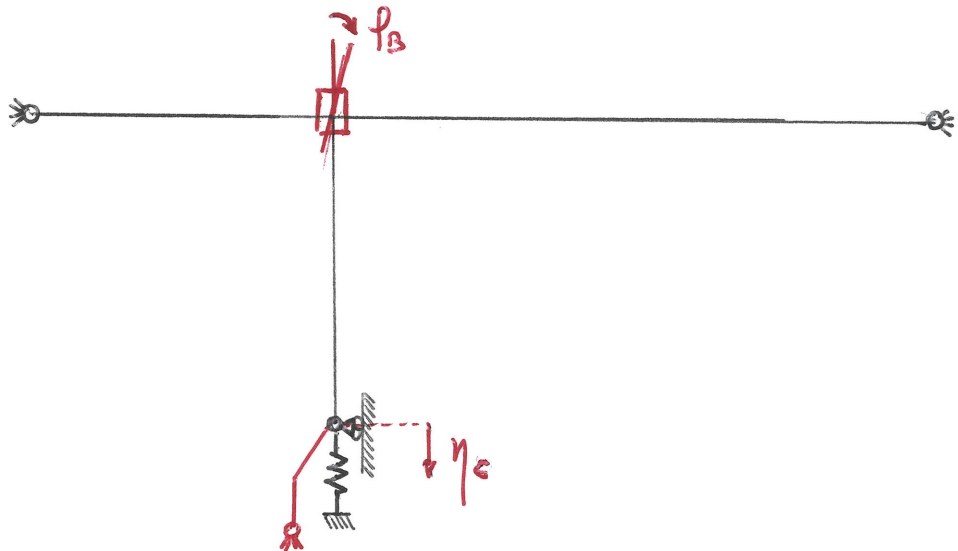
MOMENTI



AZIONI SULLE
BIELLE FINITIZIE

• Si decide di risolvere il telaio adottando il metodo degli spostamenti,
le incognite sono:

$$\begin{cases} \varphi_B \\ \eta_C \end{cases}$$

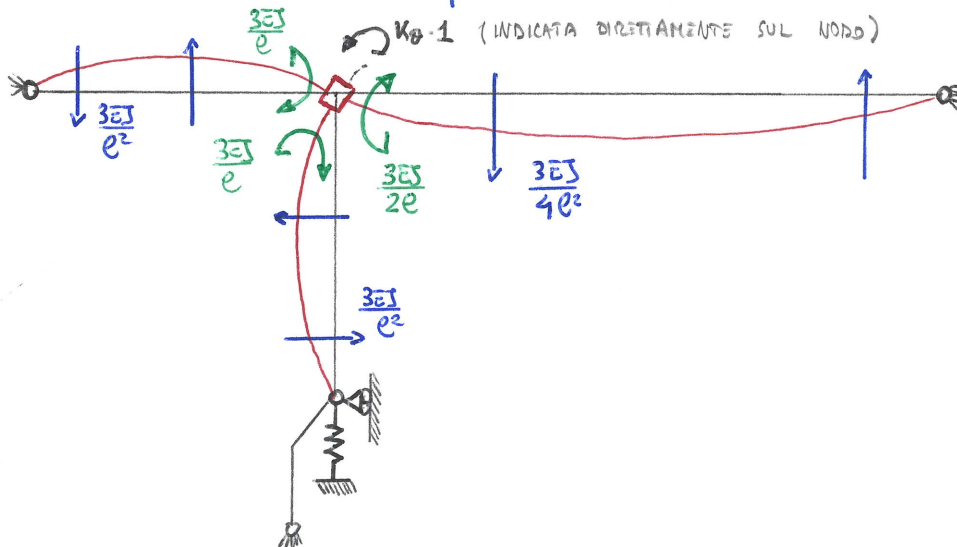


da cui il sistema risolvete (SISTEMA DELLE EQUAZIONI DI EQUILIBRIO)

$$\begin{cases} \sum M_B = 0 \\ \sum R_C = 0 \end{cases} \quad \begin{cases} M_{BB} \varphi_B + M_{BC} \eta_C + M_{BP} = 0 \\ h_{CB} \varphi_B + h_{CC} \eta_C + h_{CO} = 0 \end{cases}$$

* CASO 1:

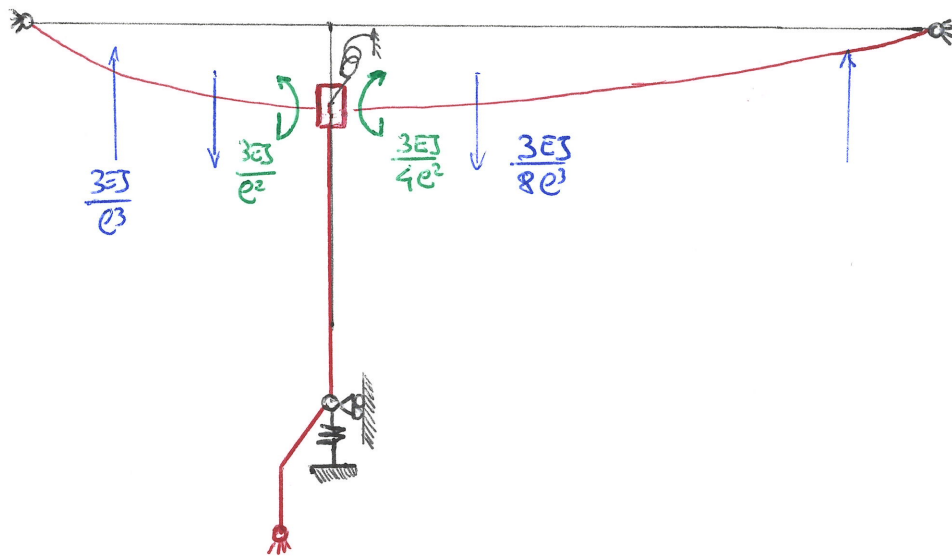
$$\varphi_B = 1; \eta_C = 0; \forall P_{ext} = 0$$



$$\begin{aligned} M_{BB} &= K_\theta + \left(\frac{3}{2} + 3 + 3 \right) \frac{EI}{e} \\ &= \frac{43}{4} \frac{EI}{e} \end{aligned}$$

$$h_{CB} = \frac{9}{4} \frac{EI}{e^2}$$

* CASO 2: $\varphi_B = 0$; $\eta_C = 1$; $\forall P_{ext} = 0$

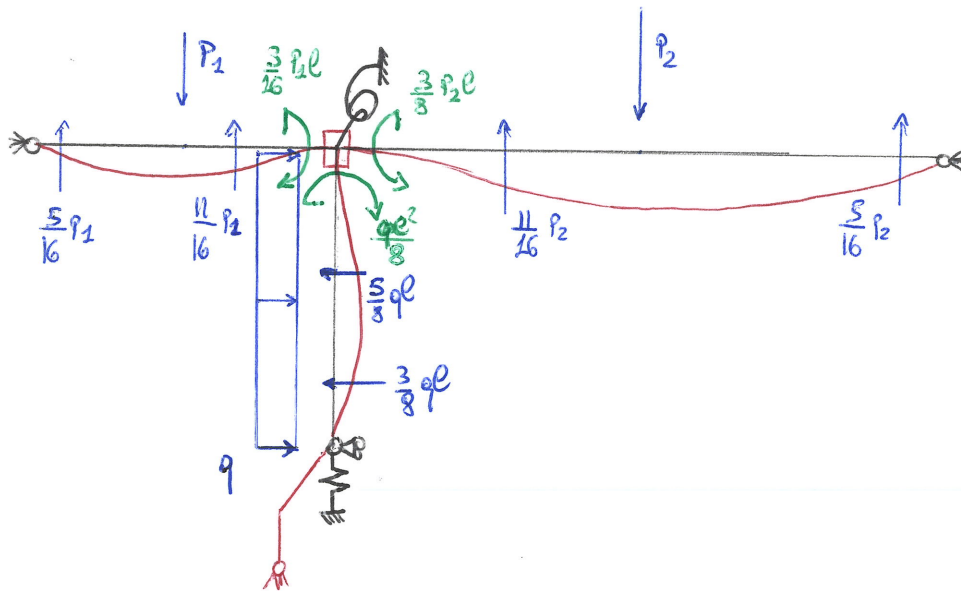


$$M_{BC} = -\frac{9}{4} \frac{EJ}{e^2}$$

$$h_{CC} = -\frac{3EJ}{e^2} - \frac{3EJ}{e^2} - \kappa_\eta$$

$$= -9 \frac{EJ}{e^2}$$

* CASO 3: $\varphi_B = 0$; $\eta_C = 0$; $\forall P_{ext} \neq 0$



$$M_{BC} = \frac{3}{16} P_1 e - \frac{3}{16} P_2 e + \frac{q e^2}{8}$$

$$= \frac{3}{4} q e^2 - \frac{13}{8} q e^2 + \frac{q e^2}{8}$$

$$= -q e^2$$

$$h_{CC} = \frac{11}{16} P_1 + \frac{11}{16} P_2$$

$$+ \frac{99}{16} q e$$

Sistema risolvete:

$$\begin{cases} \frac{43}{4} \frac{EJ}{e} \varphi_B - \frac{9}{4} \frac{EJ}{e^2} \eta_C - q e^2 = 0 & 1) \\ \frac{9}{4} \frac{EJ}{e^2} \varphi_B - 9 \frac{EJ}{e^3} \eta_C + \frac{99}{16} q e = 0 & 2) \end{cases}$$

moltiplico l'equazione 1) per $\frac{9}{43}e$ poi sottraggo la 2) dalla 1):

$$-\frac{81}{172} \frac{EJ}{e^3} \eta_c + 9 \frac{EJ}{e^3} \eta_c - \frac{9}{48} ql - \frac{99}{16} ql = 0$$

$$\rightarrow \frac{1467}{172} \frac{EJ}{e^3} \eta_c - \frac{4401}{688} ql = 0 \rightarrow \eta_c = \frac{3}{4} \frac{ql^4}{EJ}$$

Sostituisco ora η_D in 2):

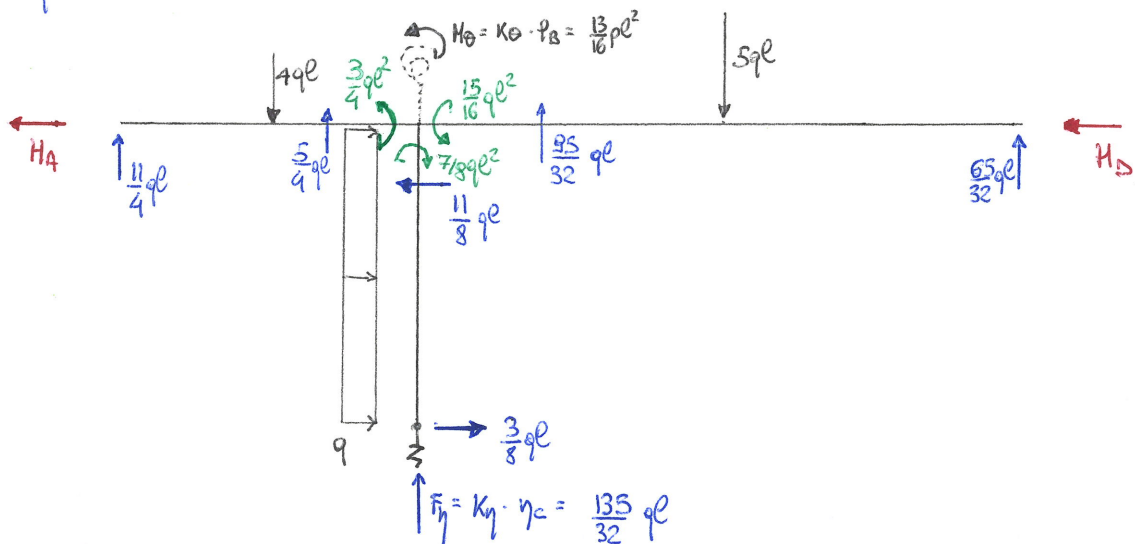
$$\frac{9}{4} \frac{EJ}{e^2} \varphi_B - 9 \frac{EJ}{e^3} \cdot \frac{3}{4} \frac{ql^4}{EJ} + \frac{99}{16} ql = 0$$

$$\rightarrow \frac{9}{4} \frac{EJ}{e^2} \varphi_B - \frac{9}{16} ql = 0 \rightarrow \varphi_B = \frac{1}{4} \frac{ql^3}{EJ}$$

Da cui in conclusione:

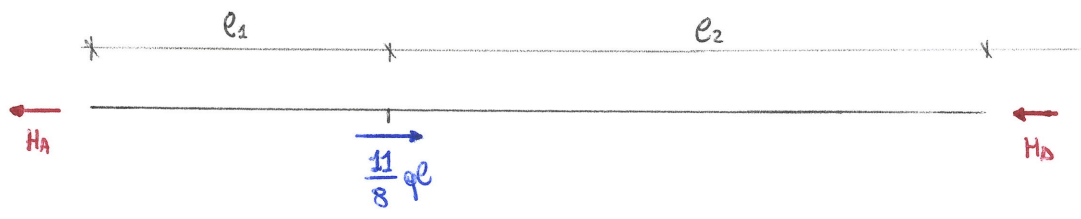
$$\begin{cases} \varphi_B = \frac{1}{4} \frac{ql^3}{EJ} \\ \eta_c = \frac{3}{4} \frac{ql^4}{EJ} \end{cases}$$

• Si passa quindi al calcolo delle azioni interne:



oss. Come ricavare il valore delle azioni esterne H_A e H_D ?

→ L'AZIONE ASSIALE ($11/8 ql$) SI RIPARTISCE IN BASE ALLE RIGIDITÀ:



$$\begin{aligned}
 H_A &= P \cdot \frac{K_1}{K_1 + K_2} \\
 &= \frac{11}{8} ql \cdot \frac{EA/l_1}{EA \cdot (\frac{1}{l_1} + \frac{1}{l_2})} \\
 &= \frac{11}{8} ql \cdot \frac{l_2}{l_1 + l_2} \\
 &= \frac{11}{8} ql \cdot \frac{2l}{3l} \\
 &= \frac{11}{12} ql
 \end{aligned}$$

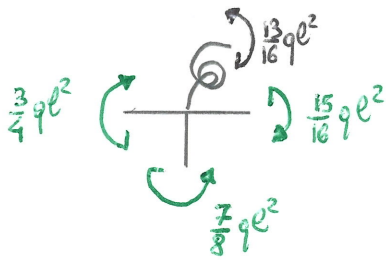
$$\begin{aligned}
 H_B &= P \cdot \frac{K_2}{K_1 + K_2} \\
 &= \frac{11}{8} ql \cdot \frac{EA/l_2}{EA \cdot (\frac{1}{l_1} + \frac{1}{l_2})} \\
 &= \frac{11}{8} ql \cdot \frac{l_1}{l_1 + l_2} \\
 &= \frac{11}{8} ql \cdot \frac{l}{3l} \\
 &= \frac{11}{24} ql
 \end{aligned}$$

A questo punto posso verificare l'equilibrio globale: $\Sigma M_c = 0$

$$\frac{11}{4} ql^2 - \frac{11}{12} ql^2 - 2 ql^2 - \frac{13}{16} ql^2 + \frac{ql^2}{2} + 5 ql^2 - \frac{65}{16} ql^2 - \frac{11}{24} ql^2 \stackrel{?}{=} 0$$

$$0 = 0 \quad \checkmark$$

Verifica dell'equilibrio locale nel nodo in B: $\Sigma M_B^{locl} = 0$



$$\frac{3}{4} ql^2 + \frac{15}{16} ql^2 - \frac{7}{8} ql^2 - \frac{13}{16} ql^2 \stackrel{?}{=} 0$$

$$0 = 0 \quad \checkmark$$

Verifica alla trazione verticale:

$$\Sigma F_v = 0$$

$$\frac{11}{4} ql - 4 ql - 5 ql + \frac{65}{32} ql + \frac{135}{32} ql \stackrel{?}{=} 0$$

$$0 = 0 \quad \checkmark$$

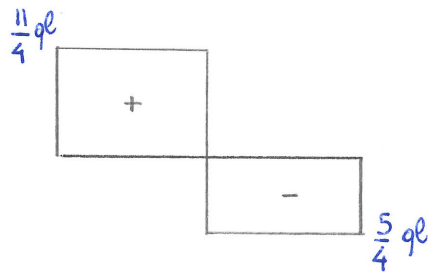
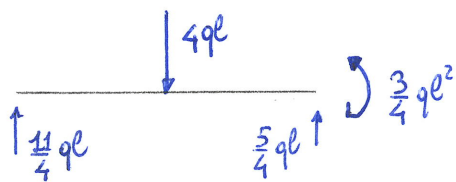
Verifica alla trazione orizzontale:

$$\Sigma F_H = 0$$

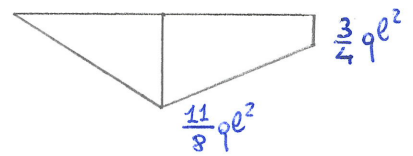
$$ql + \frac{3}{8} ql - \frac{11}{12} ql - \frac{11}{24} ql \stackrel{?}{=} 0$$

$$0 = 0 \quad \checkmark$$

ASTA AB:

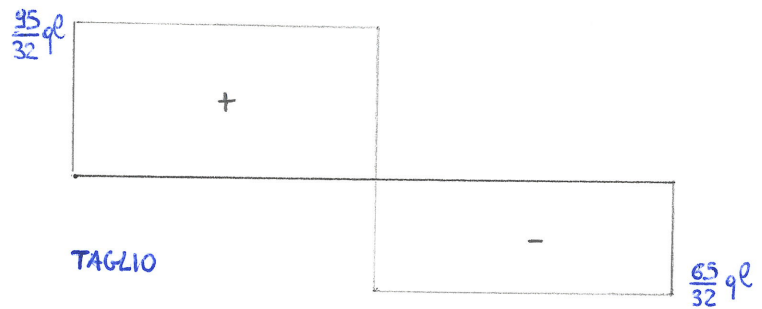
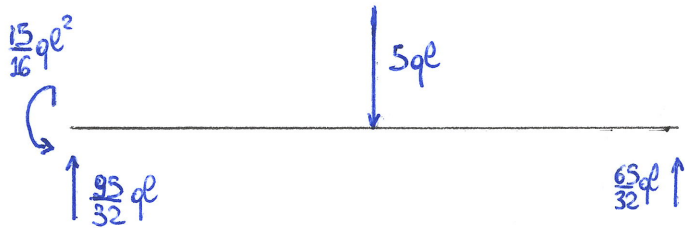


TAGLIO

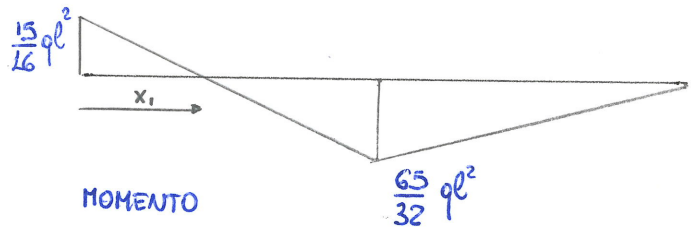


MOMENTO

ASTA BD:



TAGLIO

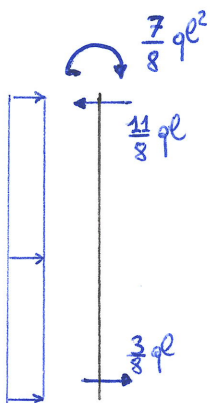


MOMENTO

$$\frac{15}{16} : x_1 = \frac{95}{32} : l$$

$$x_1 = \frac{6}{13} l$$

ASTA BC:



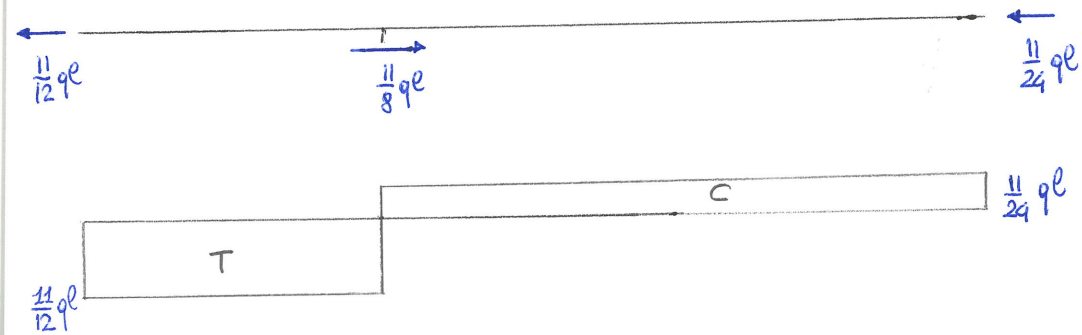
TAGLIO



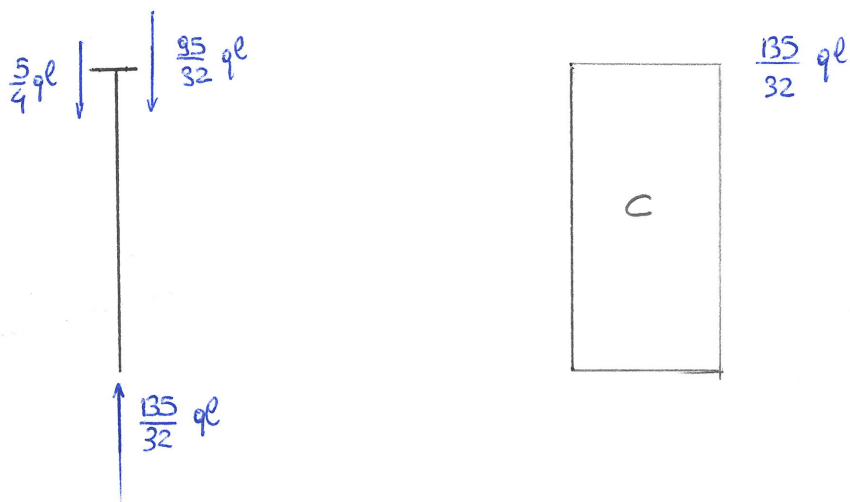
MOMENTO

Azioni assiali:

ASTE AB + BD



ASTA BC



• Grafici finali:

