

TECNICA DELLE COSTRUZIONI

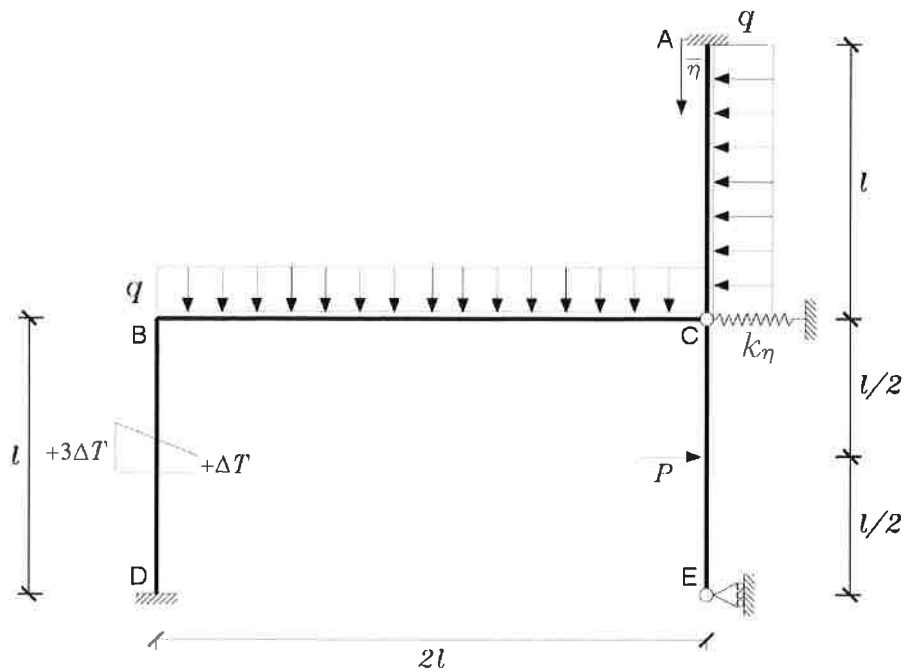
TEMA ESAME DEL 10 LUGLIO 2018

DOCENTI: PROF. GIOVANNI PLIZZARI
PROF. FAUSTO MINELLI

ESERCITATORE: ING. LUCA FACCONI

DURATA: 2 ORE

Esercizio



$$K_n = \frac{7 EJ}{2 l^3}$$

$$\bar{n} = \frac{ql^4}{EJ}$$

$$P = ql$$

$$\alpha \Delta T = \frac{1 ql^3}{4 EJ}$$

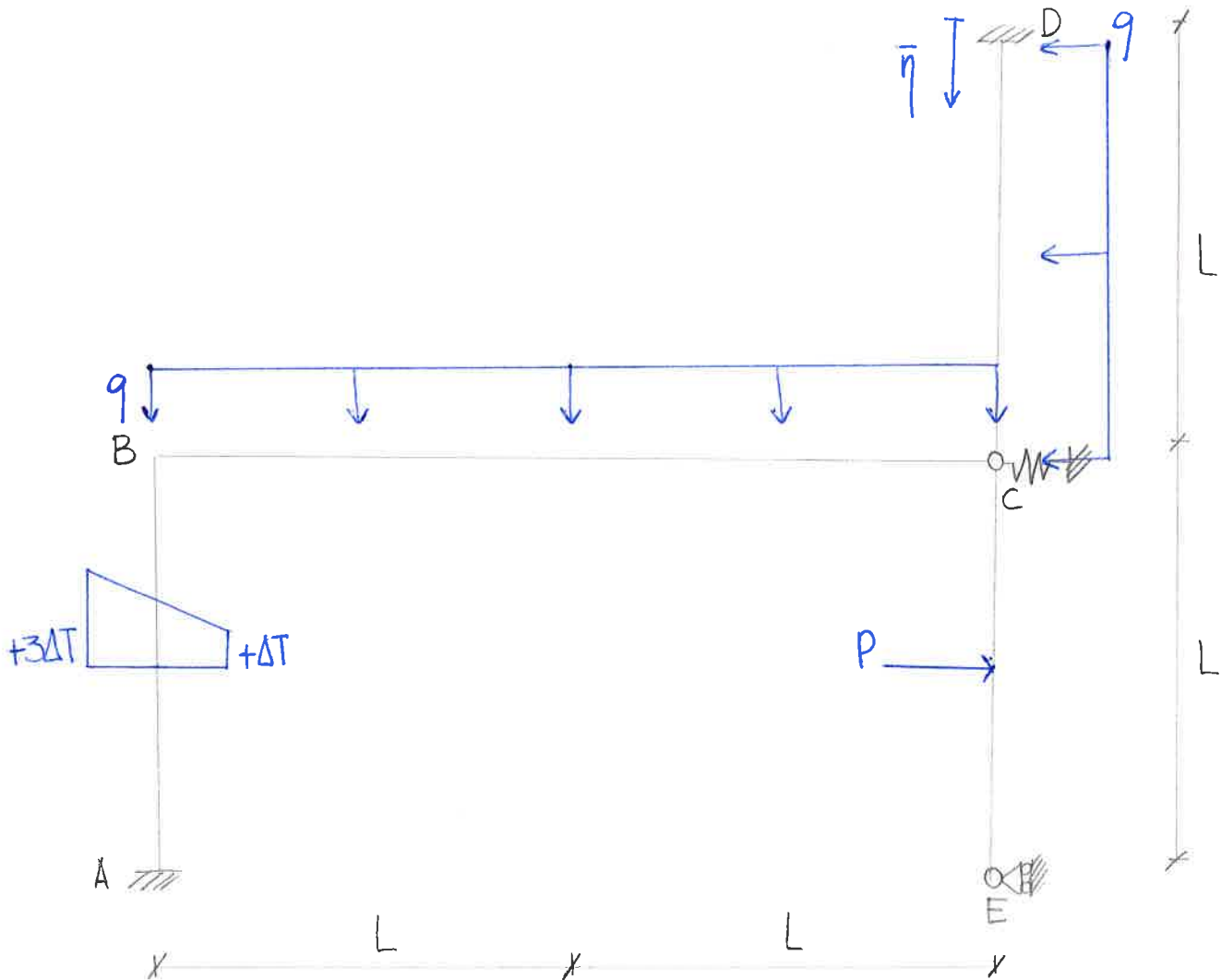
$$\frac{\alpha \Delta T}{H} = \frac{1 ql^2}{2 EJ}$$

Dato il telaio in figura, si richiedono i grafici di:

1. Momento flettente (con il valore e la posizione dei massimi);
2. Taglio;
3. Azione assiale;
4. Deformata qualitativa con posizione dei flessi.

Quanto richiesto, ed i calcoli necessari per lo sviluppo del tema, vanno riportati nello stesso in maniera chiara e con tratto non cancellabile.

TEMA ESAME 10/07/2018



DATI

$$k_{\eta} = \frac{7}{2} \frac{EJ}{L}$$

$$\Delta T = \frac{1}{4} \frac{qL^3}{EJ}$$

$$\bar{\eta} = \frac{qL^4}{EJ}$$

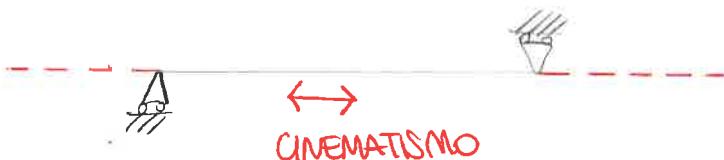
$$\frac{\Delta T}{H} = \frac{1}{2} \frac{qL^2}{EJ}$$

$$P = qL$$

NSI VALUTA IL GRADO DI IPERSTATICITÀ DELLA STRUTTURA

$$\left. \begin{array}{l} GdV = 12 \\ GdL = 9 \end{array} \right\} 3 \text{ VOLTE IPERSTATICA}$$

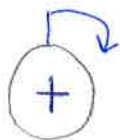
NSI OSSERVA CHE IL TELAIÒ È A NODI SPOTABILI → BIELLA FITTA IN C



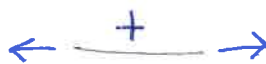
N CONVENZIONE DI SEGNO



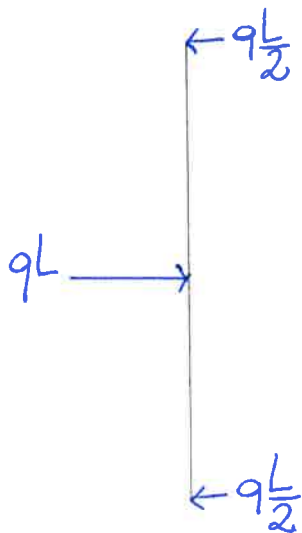
MOMENTI AL NODO



ROTAZIONI



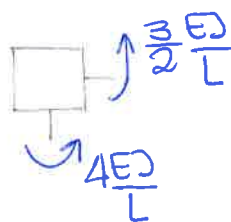
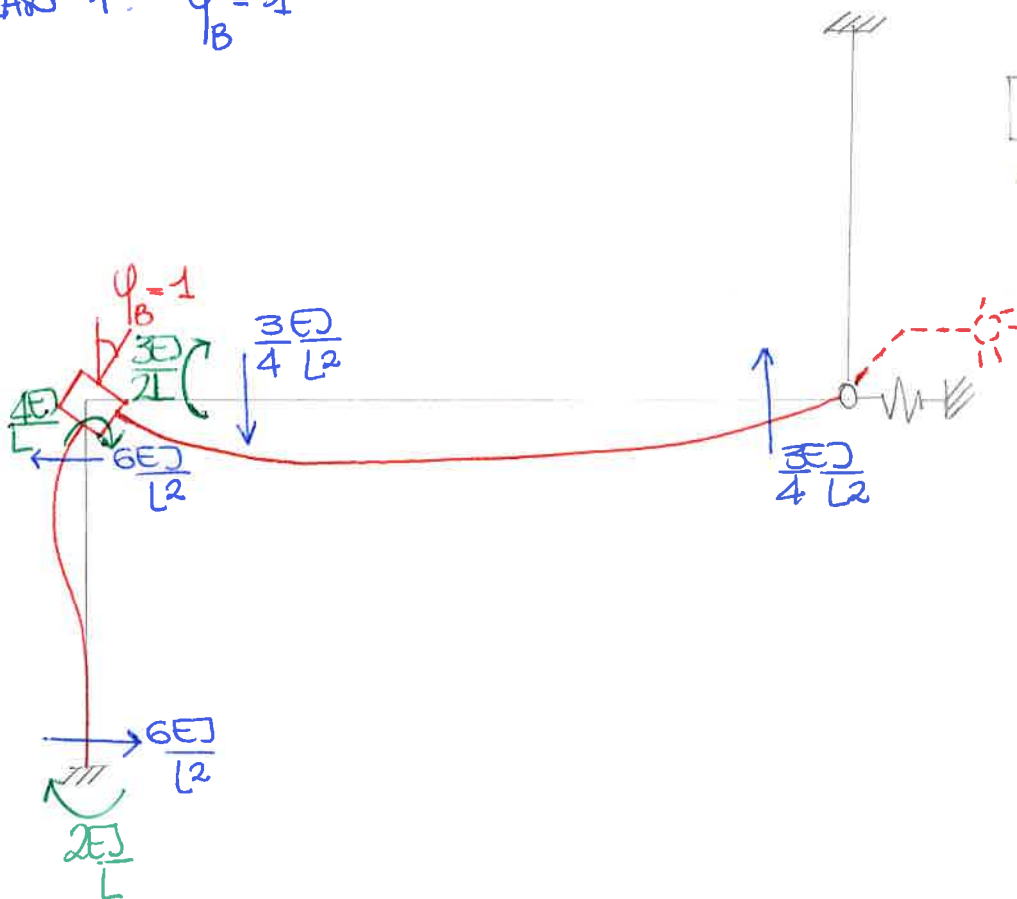
N APPENDICE ISOSTATICA CE



N SISTEMA RISOLVENTE

$$\begin{cases} m_{BB} \varphi_B + m_{BC} \eta_C + m_{B0} = 0 \\ h_{CB} \varphi_B + h_{CC} \eta_C + h_{C0} = 0 \end{cases}$$

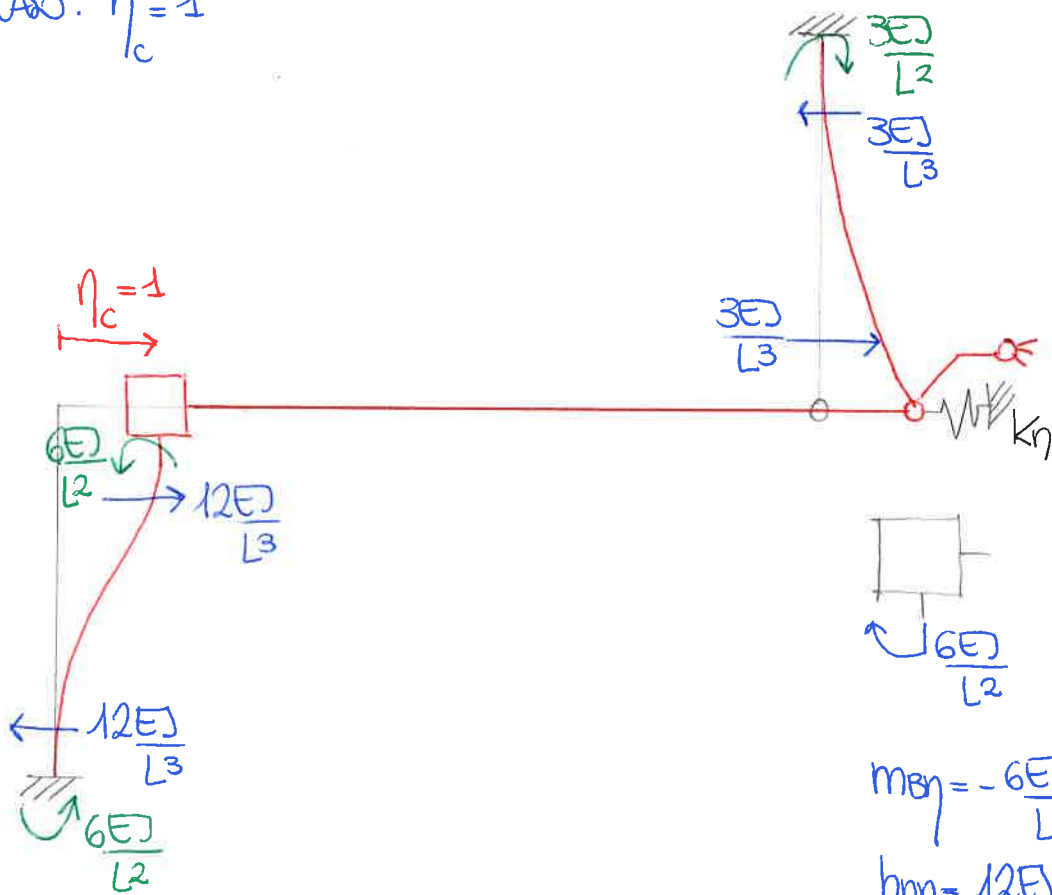
* CASO 1: $\varphi_B = 1$



$$m_{BB} = 4EJ/L + 3EJ/(2L) = 11EJ/(2L)$$

$$h_{CB} = -6EJ/L^2$$

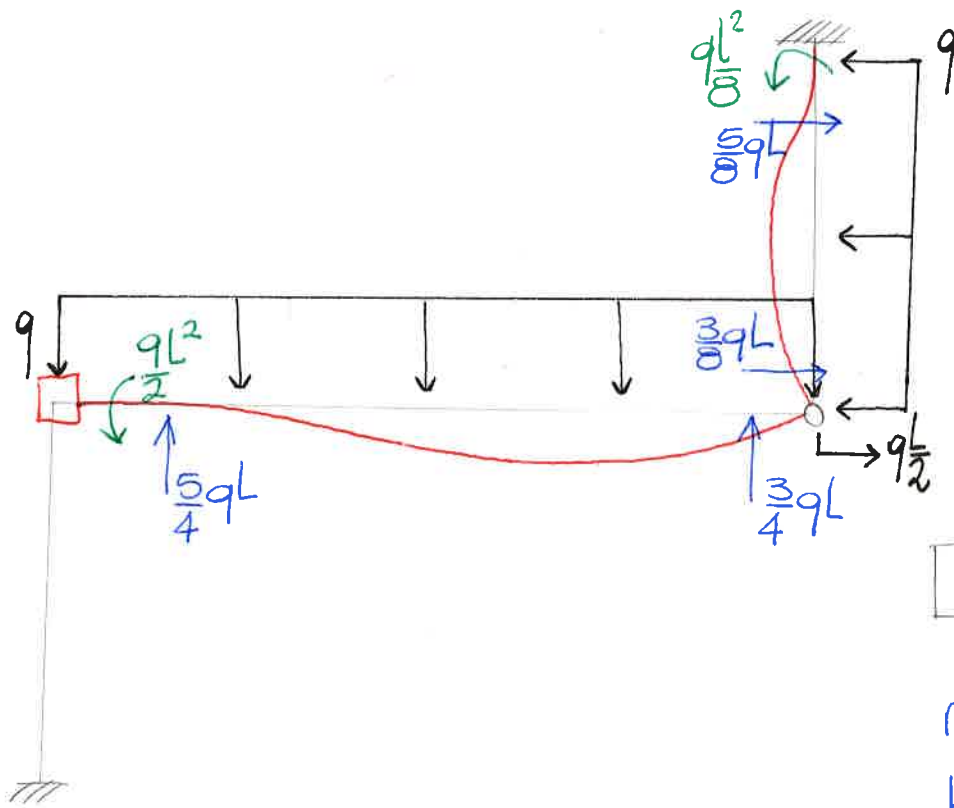
* 2 caso: $\eta_c = 1$



$$m_{B\eta} = -\frac{6EJ}{L^2}$$

$$h_{\eta\eta} = \frac{12EJ}{L^3} + \frac{3EJ}{L^3} + \frac{7}{2} \frac{EJ}{L^3} = \frac{37EJ}{2L^3}$$

* caso 3: $q \neq 0$

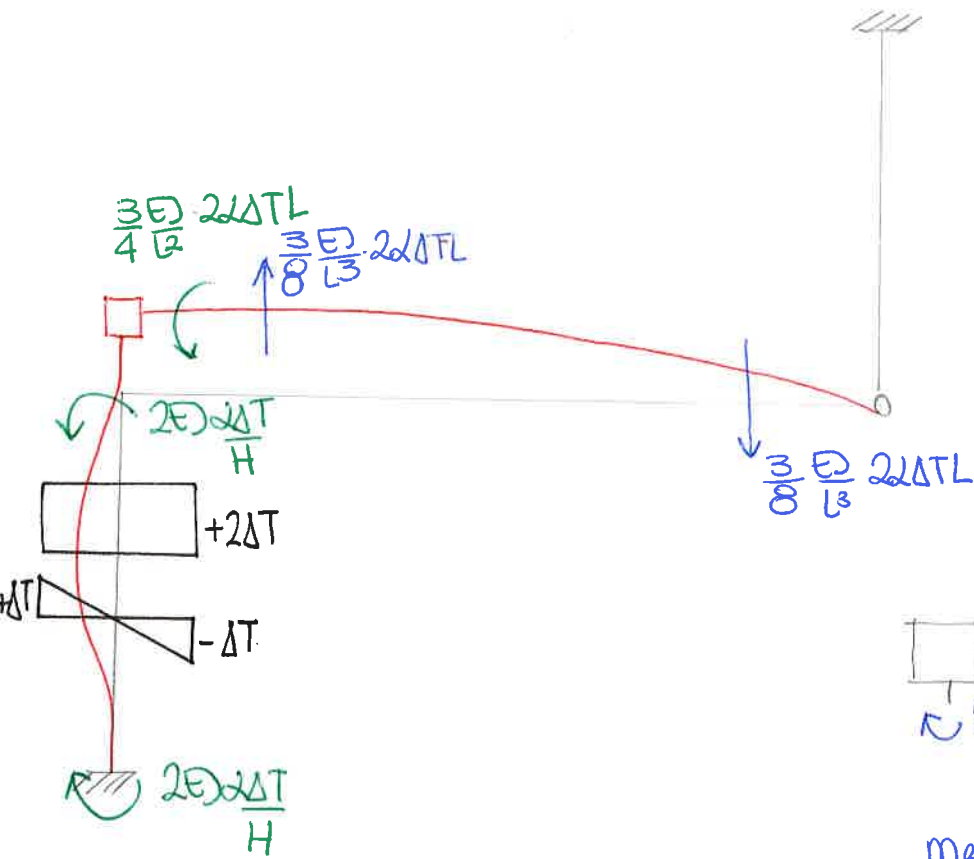


$$m_{B,1} = -\frac{qL^2}{2}$$

$$h_{\eta,1} = -q\frac{L}{2} + \frac{3}{8}qL - \frac{1}{8}qL$$

$$h_{\eta,1} = -q\frac{L}{2} + \frac{3}{8}qL - \frac{1}{8}qL$$

* CASO 4 $\Delta T \neq 0$

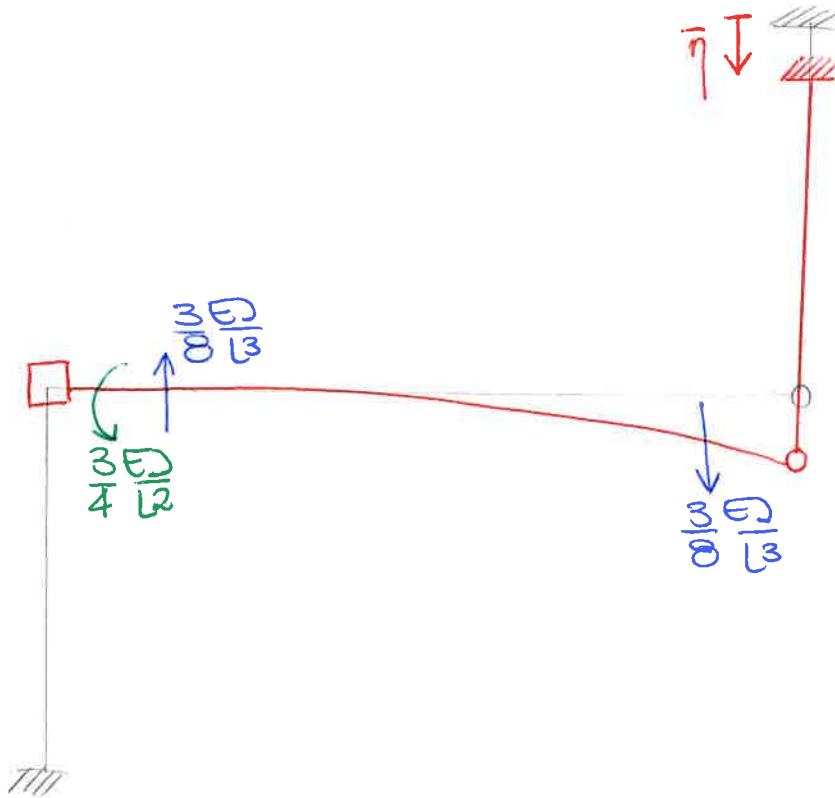


$$\begin{aligned} \square \rightarrow & \frac{3E}{4L^2} 2\Delta T = \frac{3}{8} qL^2 \\ \curvearrowright & 2E \Delta T \frac{\Delta T}{H} = qL^2 \end{aligned}$$

$$M_{B0,2} = -qL^2 - \frac{3}{8} qL^2 = -\frac{11}{8} qL^2$$

$$h_{\eta 0,2} = 0$$

* CASO 5 $\eta \neq 0$



$$\square \rightarrow \curvearrowright \frac{3E}{4L^2} \cdot \eta$$

$$M_{B0,3} = -\frac{3}{4} qL^2$$

$$h_{\eta 0,3} = 0$$

$$M_{B0} = -\frac{qL^2}{2} - \frac{11}{8}qL^2 - \frac{3}{4}qL^2 = -\frac{21}{8}qL^2$$

$$h_{p0} = -\frac{1}{8}qL$$

N SISTEMA RIDUENTE

$$\begin{cases} \frac{11}{2} \frac{EJ}{L} \varphi_B - \frac{6EJ}{L^2} \eta_c - \frac{21}{8} qL^2 = 0 & (1) \\ -\frac{6EJ}{L^2} \varphi_B + \frac{37}{2} \frac{EJ}{L^3} \eta_c - \frac{1}{8} qL = 0 & (2) \end{cases}$$

MULTIPICO (2) PER $\frac{11}{12} L$ E LA SOMMO A (1)

$$-\frac{11}{2} \frac{EJ}{L} \varphi_B + \frac{407}{24} \frac{EJ}{L^2} \eta_c - \frac{11}{96} qL^2 = 0$$

(+)

$$\frac{11}{2} \frac{EJ}{L} \varphi_B - \frac{6EJ}{L^2} \eta_c - \frac{21}{8} qL^2 = 0$$

$$\left[\frac{11}{2} \frac{EJ}{L} + \frac{11}{2} \frac{EJ}{L} \right] \varphi_B + \left[\frac{407}{24} \frac{EJ}{L^2} - \frac{6EJ}{L^2} \right] \eta_c + \left[-\frac{11}{96} qL^2 - \frac{21}{8} qL^2 \right] = 0$$

$$\frac{263}{24} \frac{EJ}{L^2} \eta_c = \frac{263}{96} qL^2$$

$$\eta_c = \frac{263}{96} qL^2 \cdot \frac{24}{263} \frac{L^2}{EJ} \rightarrow \eta_c = \frac{1}{4} \frac{qL^4}{EJ}$$

SOSTITUISCO η_c NELLA (2)

$$-\frac{6EJ}{L^2} \varphi_B + \frac{37}{2} \frac{EJ}{L^3} \cdot \frac{1}{4} \frac{qL^4}{EJ} - \frac{1}{8} qL = 0$$

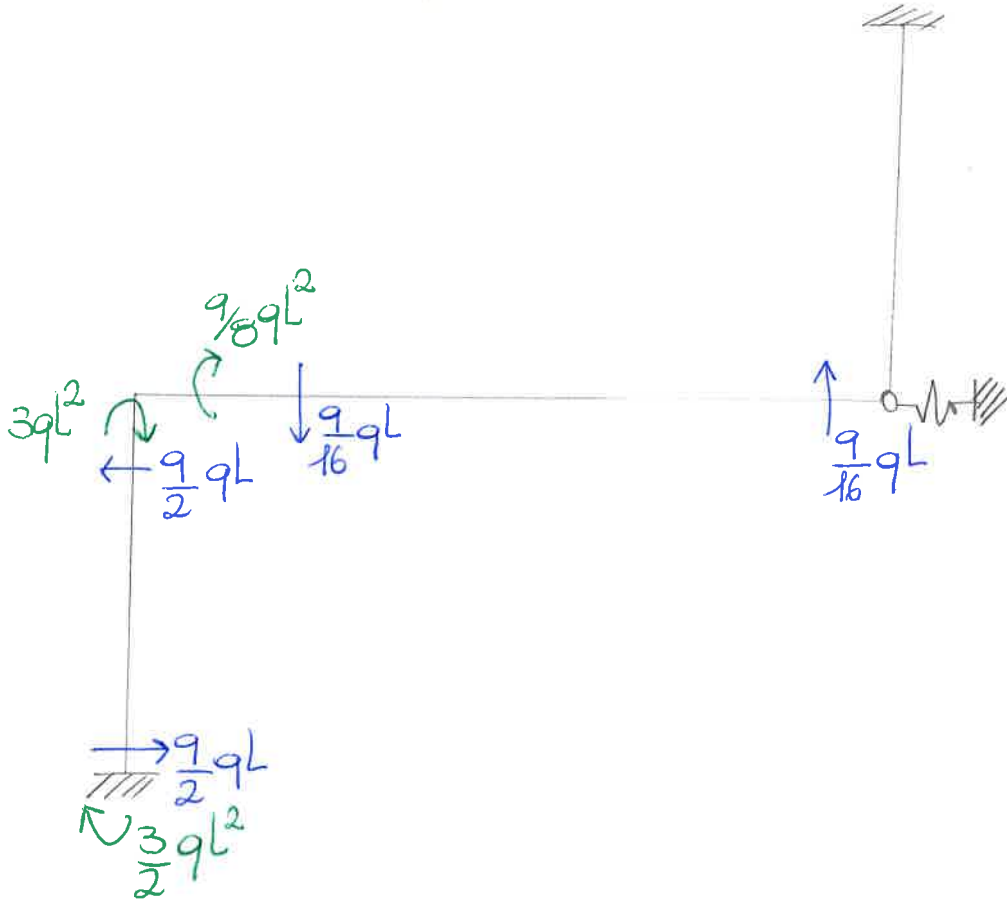
$$\frac{6EJ}{L^2} \varphi_B = \frac{36}{8} qL$$

$$\varphi_B = \frac{36}{8} qL \cdot \frac{L^2}{6EJ} \rightarrow \varphi_B = \frac{3}{4} \frac{qL^3}{EJ}$$

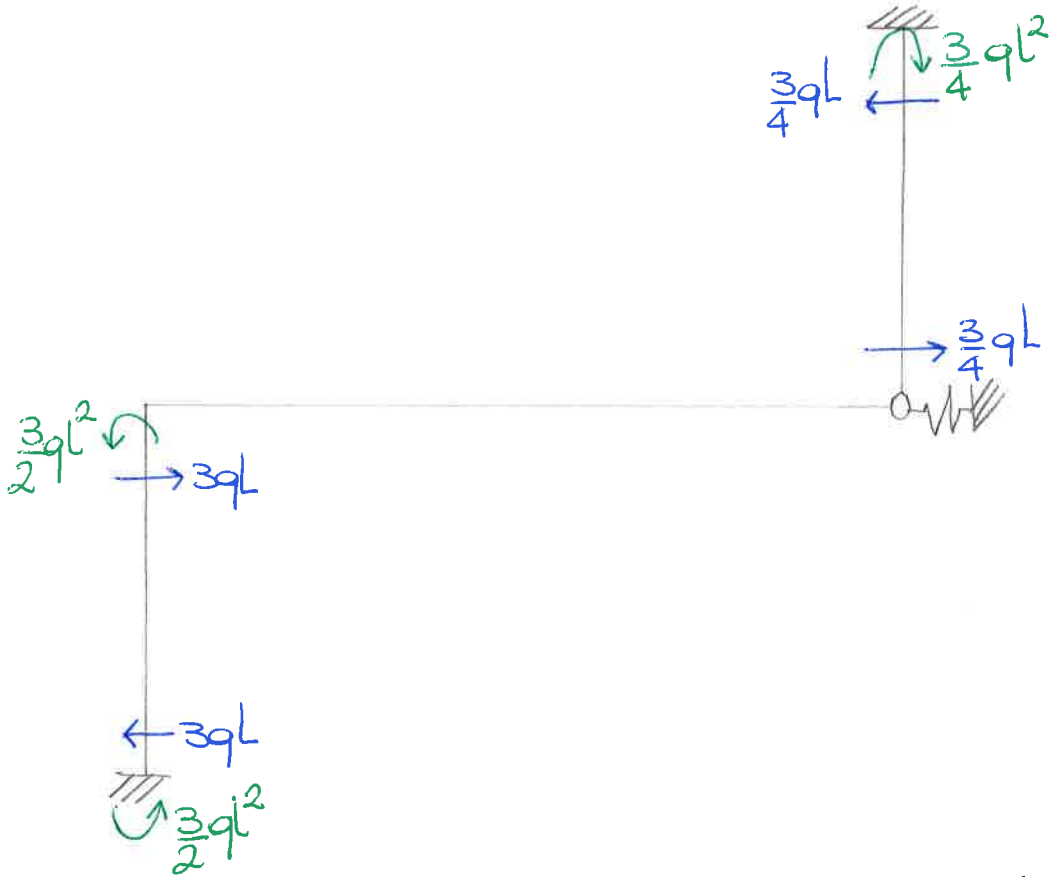
IN CONCLUSION

$$\begin{cases} \varphi_B = \frac{3}{4} \frac{qL^3}{EI} \\ \eta_C = \frac{1}{4} \frac{qL^4}{EI} \end{cases}$$

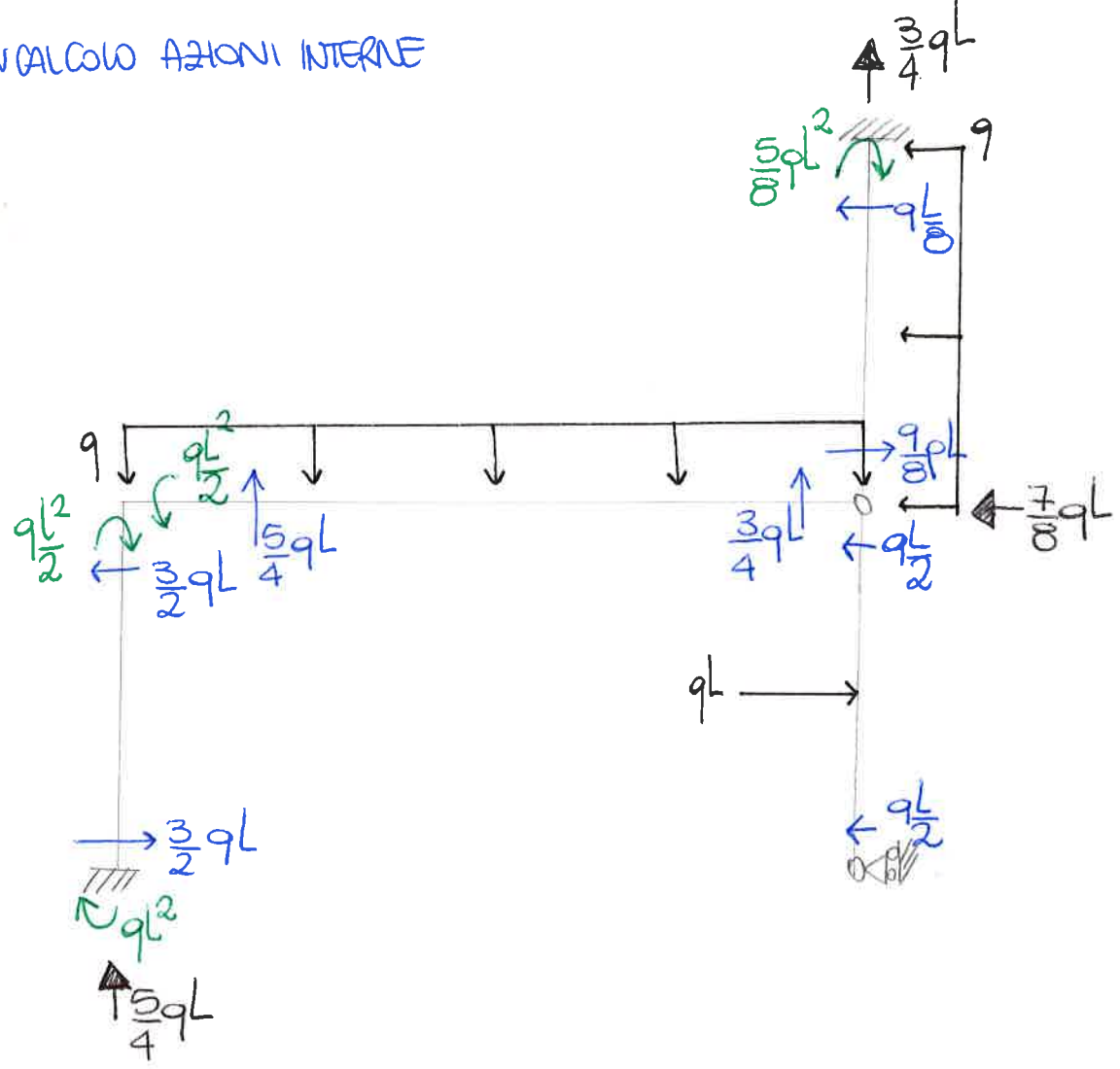
$$\approx \varphi_B = \frac{3}{4} \frac{qL^3}{EI}$$



$$N\eta_c = \frac{1}{4} \frac{ql^4}{EI}$$



NGALCOW AZHONI INTERNE



$$\text{EQ: } \uparrow + = 0$$

$$\frac{5}{4}qL - 2qL + \frac{3}{4}qL = 0 \quad \text{ok!}$$

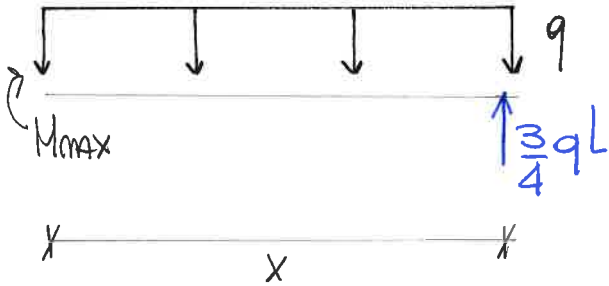
$$\text{EQ: } \rightarrow = 0$$

$$\frac{3}{2}qL + qL - q\frac{L}{2} - qL - \frac{7}{8}qL - q\frac{L}{8} = 0 \quad \text{ok!}$$

$$\text{EQ: } \uparrow B = 0$$

$$qL^2 - \frac{3}{2}qLL + q2L \cdot L - \frac{3}{4}qL \cdot 2L - qL\frac{L}{2} - q\frac{L}{8} \cdot L + \frac{5}{8}qL = 0 \quad \text{ok!}$$

N MOMENTO MASSIMO

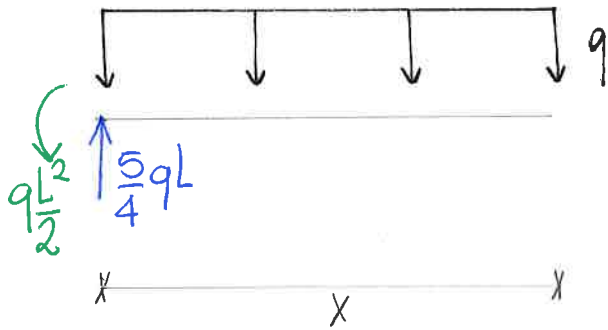


$$+\frac{3}{4}qL \cdot x - q \cdot x \cdot \frac{x}{2} = M_{max}$$

$$\frac{dM_{max}}{dx} = +\frac{3}{4}qL - qx = 0 \rightarrow x = \frac{3}{4}L$$

$$M_{max} = +\frac{3}{4}qL \cdot \frac{3}{4}L - q \cdot \frac{9}{16} \frac{L^2}{2} = \frac{9}{32} qL^2$$

N FLESSO 1

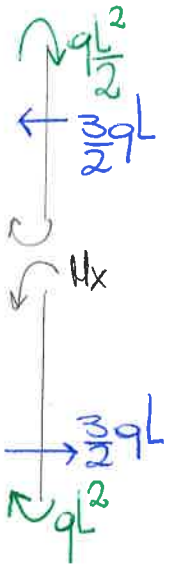


$$M = \frac{5}{4}qLx - q\frac{L^2}{2} - q\frac{x^2}{2} = 0$$

$$\frac{x^2}{2} - \frac{5}{4}xL + \frac{L^2}{2} = 0$$

$$x_{1,2} = \frac{5L \pm \sqrt{25L^2 - 16L^2}}{4} = \frac{5L \pm 3L}{4} \begin{cases} 4L \\ \frac{L}{2} \end{cases} \rightarrow x_1 = \frac{L}{2}$$

N FLESSO 2



$$y'' = -\frac{N(x)}{E} + 2 \cdot \frac{\alpha \Delta T}{H}$$

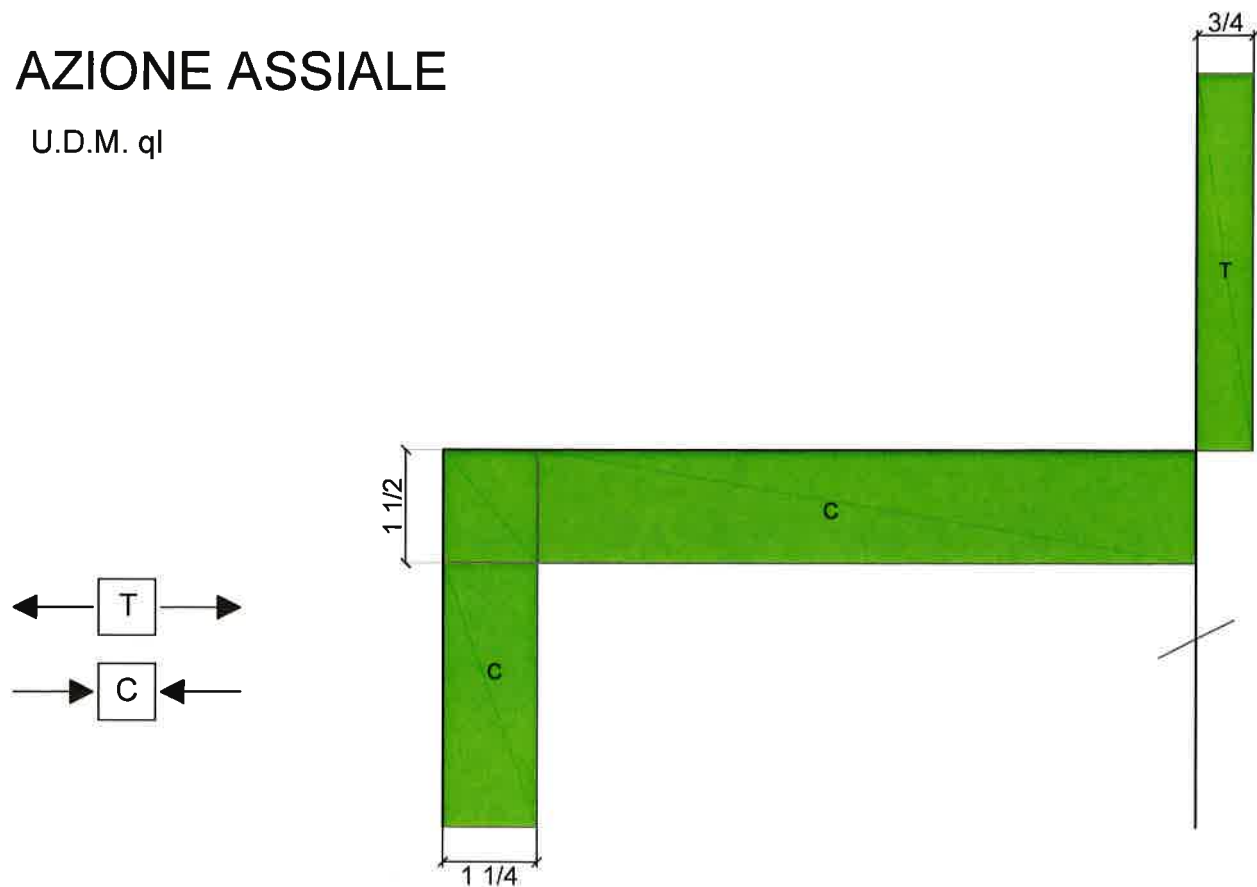
$$N(x) = -\frac{3}{2}qLx + qL^2$$

$$y'' = \frac{\frac{3}{2}qLx - qL^2}{E} + 2 \cdot \frac{\frac{1}{2}qL^2}{E}$$

$$\frac{3}{2}qLx - qL^2 + qL^2 > 0 \rightarrow x > 0 \quad \forall x$$

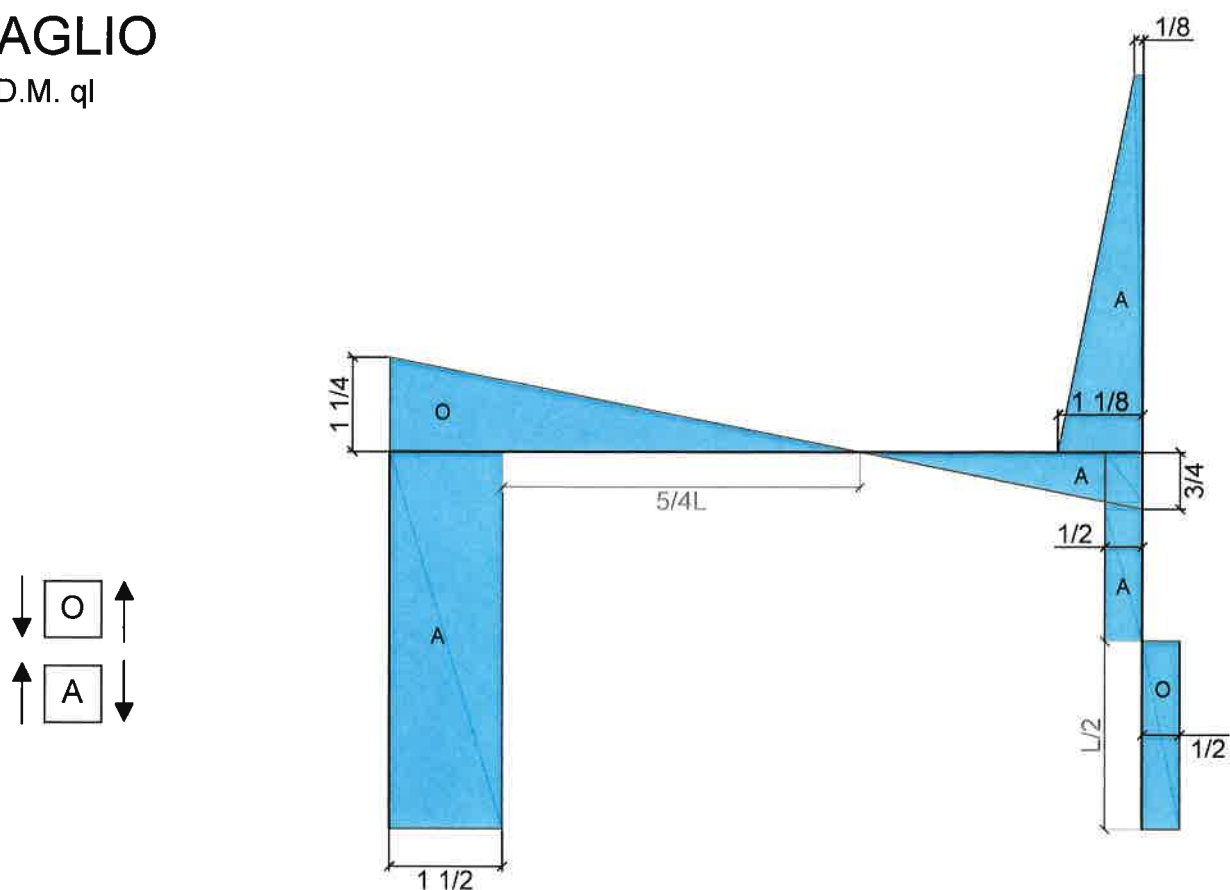
AZIONE ASSIALE

U.D.M. ql



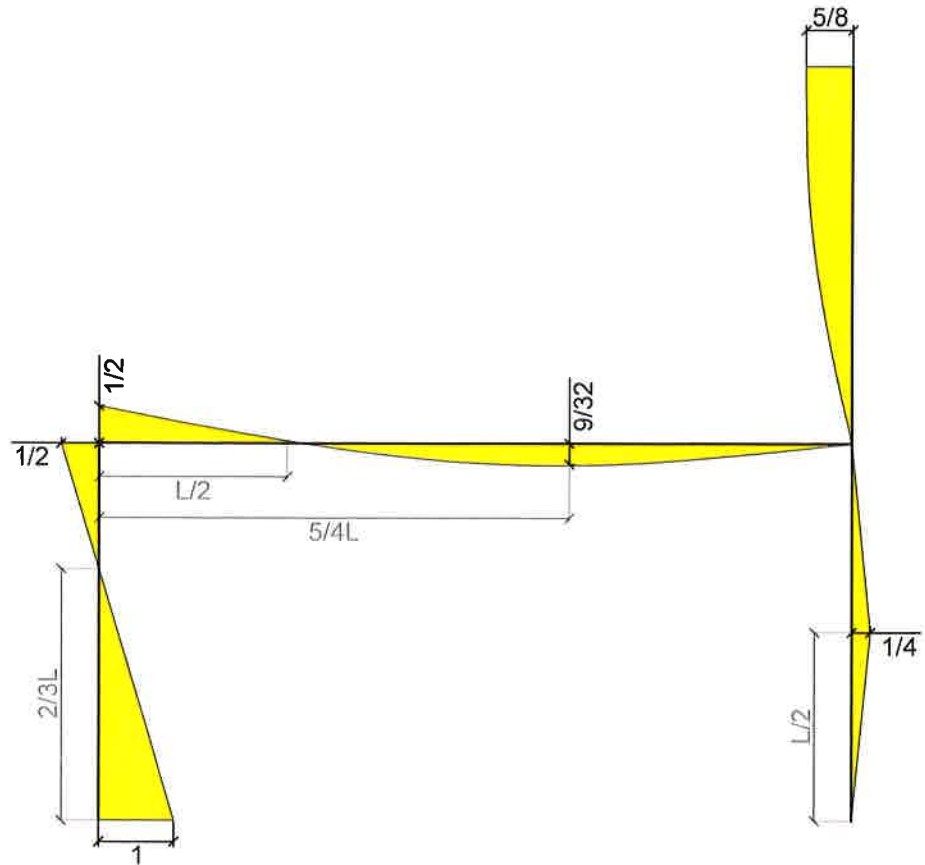
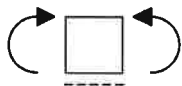
TAGLIO

U.D.M. ql



MOMENTO FLETTENTE

U.D.M. ql^2



DEFORMATA QUALITATIVA

U.D.M. Spostamenti ql^4/EJ

U.D.M. Rotazioni ql^3/EJ

U.D.M. Posizione flessi I

